

### **Bryant Development and Review Committee Meeting**

Boswell Municipal Complex - City Hall Conference Room 210 SW 3rd Street

Date: October 31, 2024 - Time: 9:00 AM

Call to Order

**Old Business** 

#### **New Business**

#### 1. 104 Rich Street - Conditional Use Permit - Accessory Structure

Steven Wise - Requesting Approval for CUP for Accessory Structure that exceeds 25% Sqft of the Primary Structure

· 0924-APP-01.pdf

#### 2. Cornerstone Montessori Christian Academy - 4910 Springhill Rd - Waiver

Hope Consulting - Requesting Waiver on Half Street Improvements until Permanent Building is built.

• 0923-LTR-01.pdf

#### 3. Hillcrest Addition Subdivision - 3927 Springhill Road

Tim Lemons - Requesting Recommendation for Preliminary Plat Approval

- · 0890-PLN-05.pdf
- 0890-RSP-04.pdf
- <u>0890-DRN-06.pdf</u>
- · 0890-DRN-05.pdf
- <u>0890-RSP-03.pdf</u>

#### 4. Parcel 840-15010-000 - Alcoa Road - Rezoning R-E to C-3

Hope Consulting - Requesting Recommendation for Rezoning from R-E to C-3

- 0922-RZNAPP-01.pdf
- 0922-RZN-02.pdf
- 0922-RZN-03.pdf
- 0922-RZNLTR-01.pdf

#### **Staff Approved**

#### 5. Window World of Little Rock - 511 Boone Road - Sign Permit

Zach Black - Requesting Sign Permit Approval - STAFF APPROVED

• 92925-SGNAPP-01.pdf

#### 6. Willow & Grace Boutique - 307 Progress Way Ste 700-800 - Sign Permit

L Graphics - Requesting Sign Permit Approval - STAFF APPROVED

• 92920-SGNAPP-01.pdf

#### 7. Bryant Mail and Print Center - 5313 HWY 5 Ste 305 - Sign Permit

L Graphics - Requesting Sign Permit Approval - STAFF APPROVED

• 92921-SGNAPP-01.pdf

#### **Permit Report**

#### **Adjournments**



# Conditional Use Permit Application

Applicants are advised to read the Conditional Use Permit section of Bryant Zoning Code prior to completing and signing this form. The Zoning Code is available at <a href="www.cityofbryant.com">www.cityofbryant.com</a> under the Planning and Community Development tab.

Date: 10/20/2024	
Applicant or Designee:	Project Location:
Name Steven Wise	Property Address 104 RICHS TREET
Address 104 RICH ST	BRYANT, AR 72023
Phone (501) 350-1410	Parcel Number
Email Address: SHYEN. WISE / (Sc)	Zoning Classification
Property Owner (If different from Applicant)	:
Name 5AME	
Phone	
Address	
Email Address	
Additional Information:	
Legal Description (Attach description if necessary  104 PICH ST	/)
Description of Conditional Use Request (Attach a	iny necessary drawings or images)  No to cover RV & Boat
see affected)	<b>→</b>
Proposed/Current Use of Property	1 DENTAL

#### **Application Checklist**

#### **Requirements for Submission**

	Letter stating request of Conditional Use and reasoning for request
	Completed Conditional Use Permit Application
	Submit Conditional Use Permit Application Fee (\$125)
	Submit Copy of completed Public Notice
	Publication: Public Notice shall be published at least one (1) time fifteen (15) days prio to the public hearing at which the variance will be heard. Once published please provide a proof of publication to the Community Development office.
	Posting of Property: The city shall provide a sign to post on the property involved for the fifteen (15) consecutive days leading up to Public hearing. One (1) sign is required for every two hundred (200) feet of street frontage.
	<ul> <li>Submit eight (8) Copies of the Development Plan (Site Plan) showing:</li> <li>Location, size, and use of buildings/signs/land or improvements</li> <li>Location, size, and arrangement of driveways and parking. Ingress/Egress</li> <li>Existing topography and proposed grading</li> <li>Proposed and existing lighting</li> <li>Proposed landscaping and screening</li> <li>Use of adjacent properties</li> <li>Scale, North Arrow, Vicinity Map</li> </ul>

Once the application is received, the material will be reviewed to make sure all the required information is provided. The applicant will be notified if additional information is required. The application will then go before the Development and Review Committee (DRC) for a recommendation

Additional information that may be requested by the administrative official due

to the Planning Commission. A public hearing will be held at this meeting for comments on the Conditional Use. After the public hearing, the Planning Commission will make a decision on the use.

Note: that this is not an exhaustive guideline regarding the Conditional Use Permit Process.

Additional information is available in the Bryant Zoning Ordinance.

**READ CAREFULLY BEFORE SIGNING** 

to unique conditions of the site.

I do hereby certify that all information contained within this application is true and correct. I further certify that the owner of the property authorizes this proposed application. I understand that I must comply with all City Codes and that it is my responsibility to obtain all necessary permits required.

TO:

City of Bryant, Arkansas

FROM:

Steven Wise, EdD

104 Rich Street

Bryant, Arkansas 72022

(501) 350-1410

steven.wise@lrsd.org

RE: Conditional Use Permit Application

Please seriously consider the attached permit for a high quality accessory structure to cover and protect my 30 ft travel trailer and boat from damages. My previous travel trailer was destroyed by falling limbs from my neighbor's large trees. I am relocating my new trailer to behind my privacy fence and installing an aesthetically pleasing awning matching the color of my house to protect my investment. I am scheduled for a major upgrade to my house in the next month and I am dedicated to improving the properties along Rich Street. Please help me keep the Heart of Bryant beating.

Thank you.

Lifetime Resident

Steven Wise

ASINACI LING -104 RICH STREET 3R/ANT, AR72022 35 24'x30' PREMIUM PAINTED CARPORT WITZIM (501) 470-0347 ROLLING GATE PRIYAC · PRIVACY



104 Rich Street
Bryant, Arkansas 72022

Owner: Steven Wise



104 Rich Street
Bryant, Arkansas 72022

Owner: Steven Wise



October 18, 2024

Colton Leonard City of Bryant 210 Southwest Third St., Bryant, AR 72022

RE: Cornerstone Montessori School (Parcel # 840-06480-002)

Dear Mr. Leonard,

On behalf of our client, please accept this request letter for a waiver for a delay in the  $\frac{1}{2}$  street improvements and trail. At this time a temporary structure has been built in an effort to quickly continue operations of this school. In the future the school has plans to build a permanent school on this property. Our request would be to delay the  $\frac{1}{2}$  street improvements and trail construction until the permanent school is built.

Sincerely,

Jonathan Hope

Hope Consulting, Inc

jonathan@hopeconsulting.com

# DETAILED PLANS:

# HILLCREST ADDITION

PART OF SECTION 12, T-4-N, R-10-W CITY OF BRYANT, SALINE COUNTY, ARKANSAS

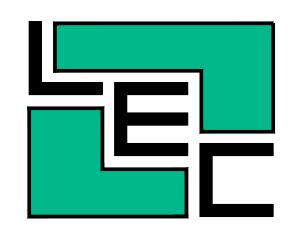
> JULY 9, 2024 REVISED: OCTOBER 24, 2024

## PREPARED FOR:

SPRINGHILL HWY 5 DEVELOPMENT, LLC 816 E. OAK STREET CONWAY, ARKANSAS 72032





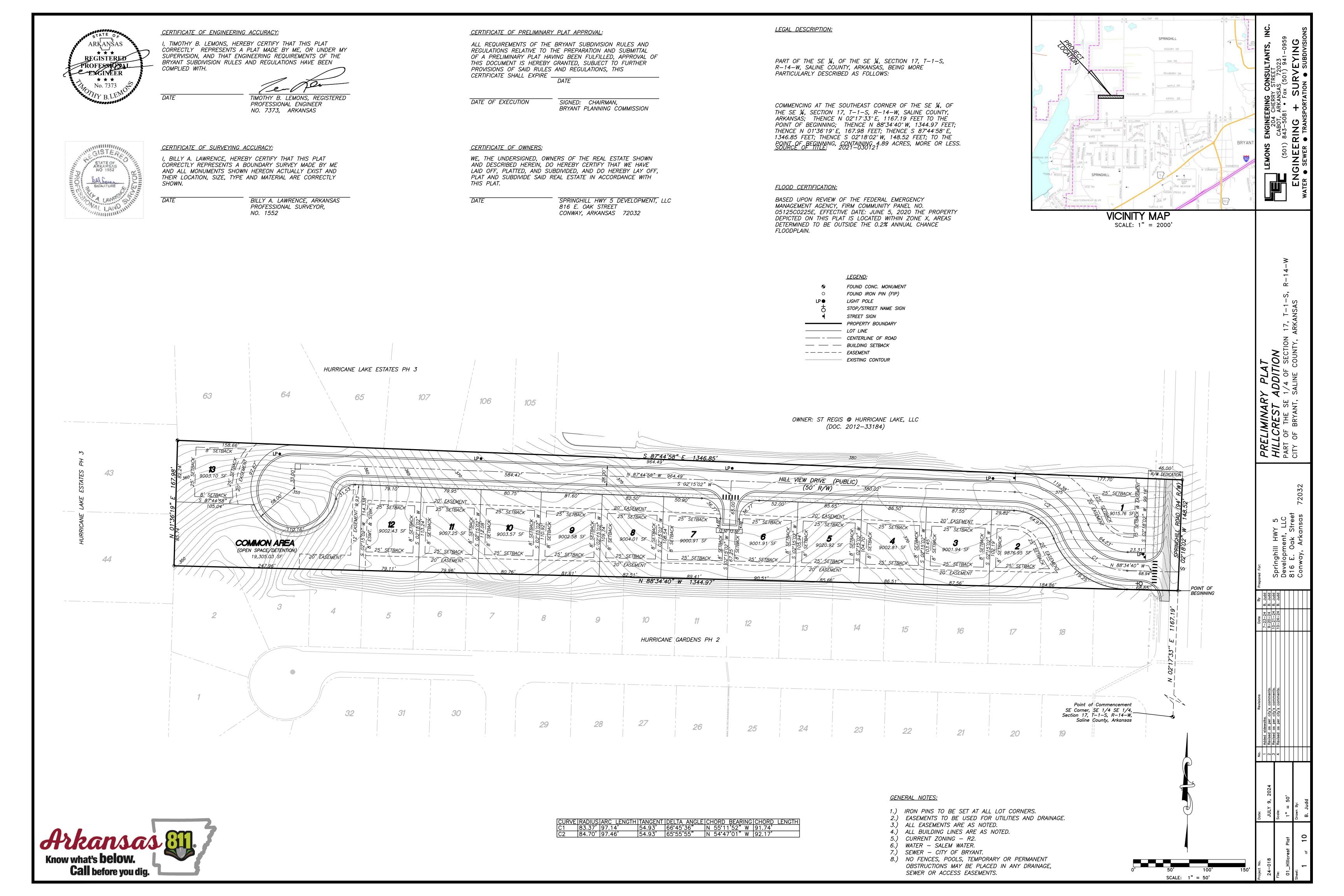


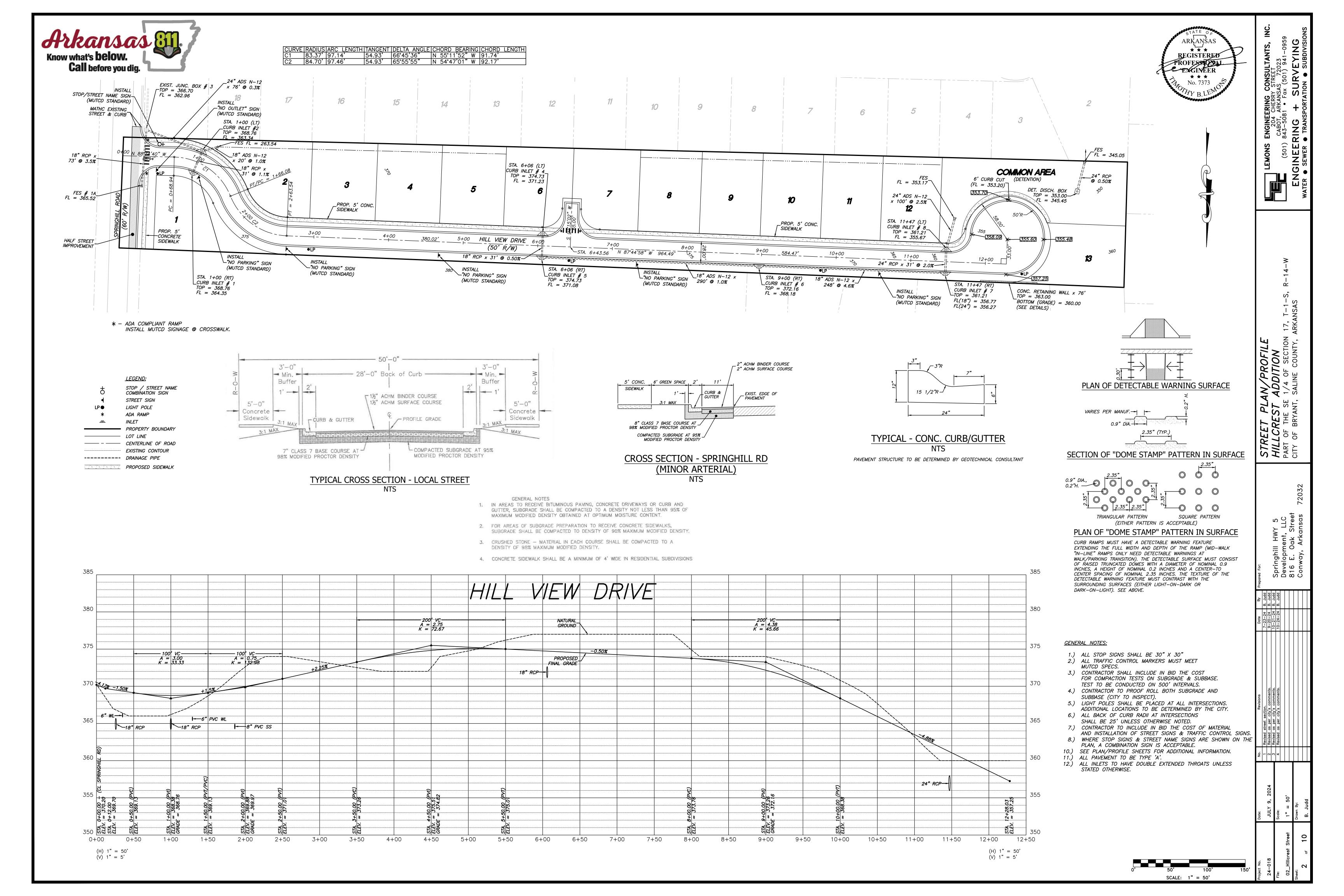
# Prepared By:

LEMONS ENGINEERING CONSULTANTS, INC. 204 CHERRY STREET CABOT, ARKANSAS 72023

ENGINEERING • SURVEYING • PLANNING

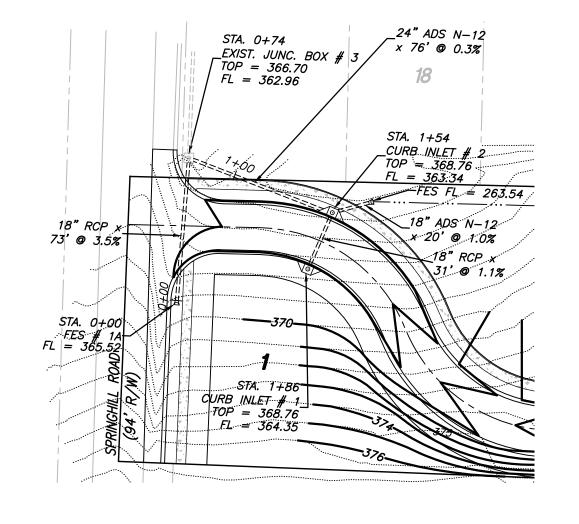
INDEX OF SHEETS	
Preliminary Plat	1
Street Plan/Profile	2
Culvert Plan/Profile	3
Grading Plan	4
Detention Pond Plan	5
Water Layout	6
Construction Details — Water	7
Sewer Plan/Profile	8
Construction Details — Sewer	9
Erosion Control Plan	10

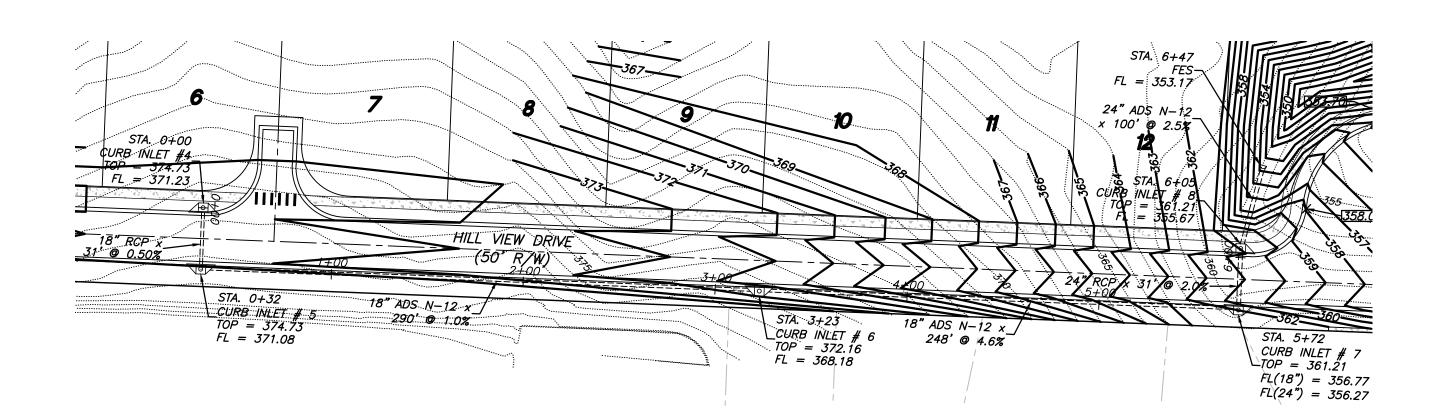


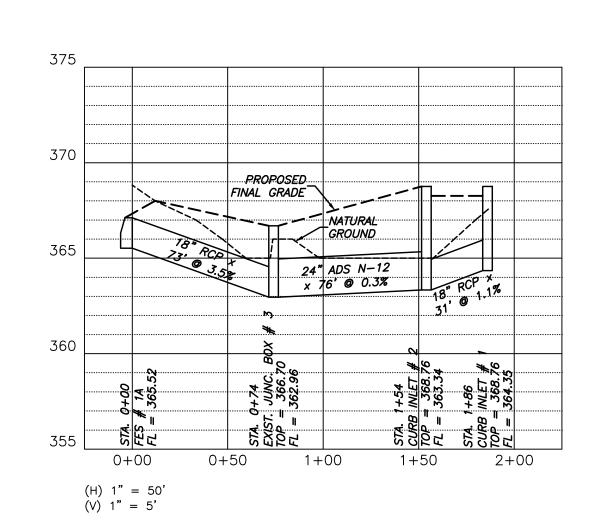


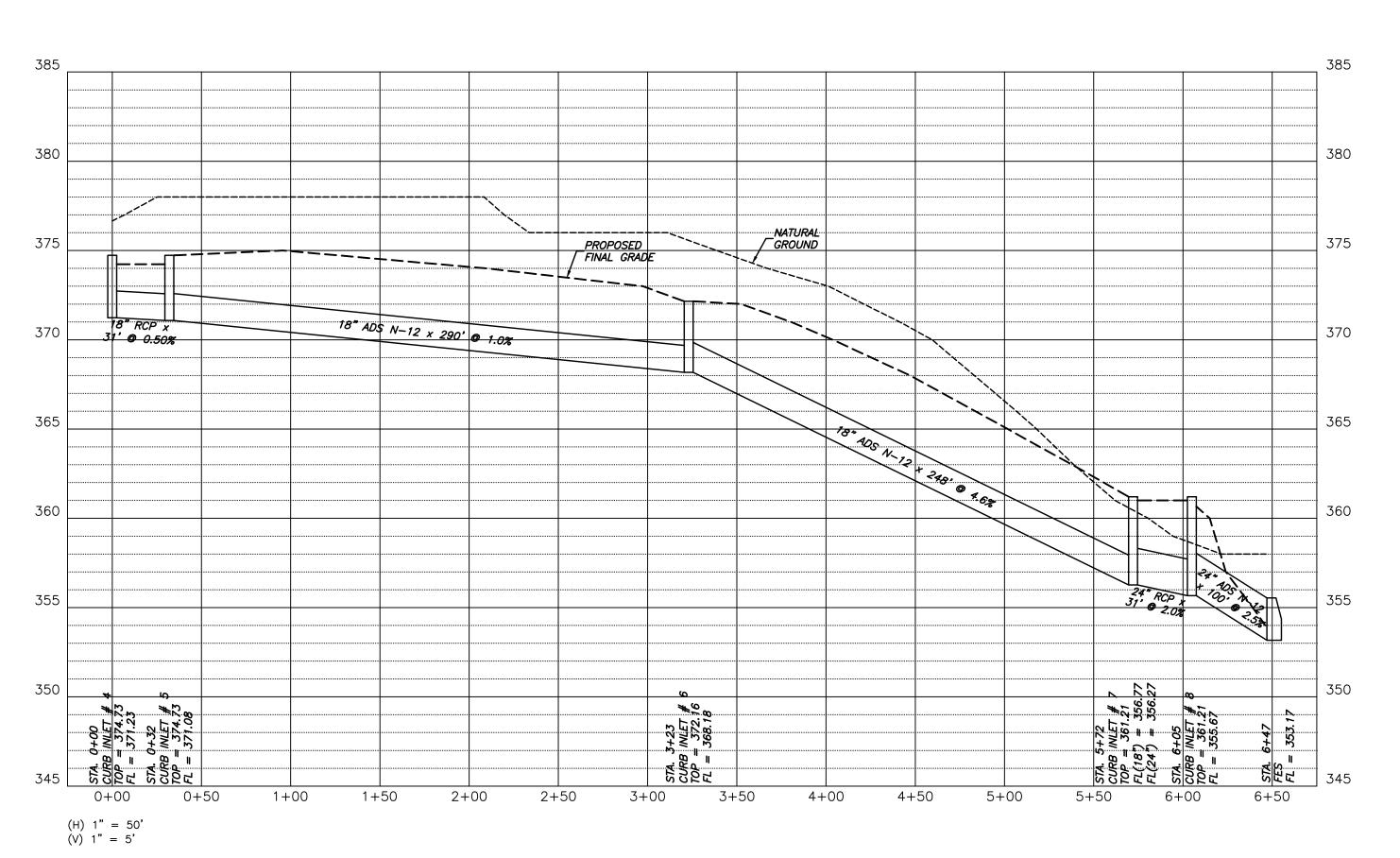










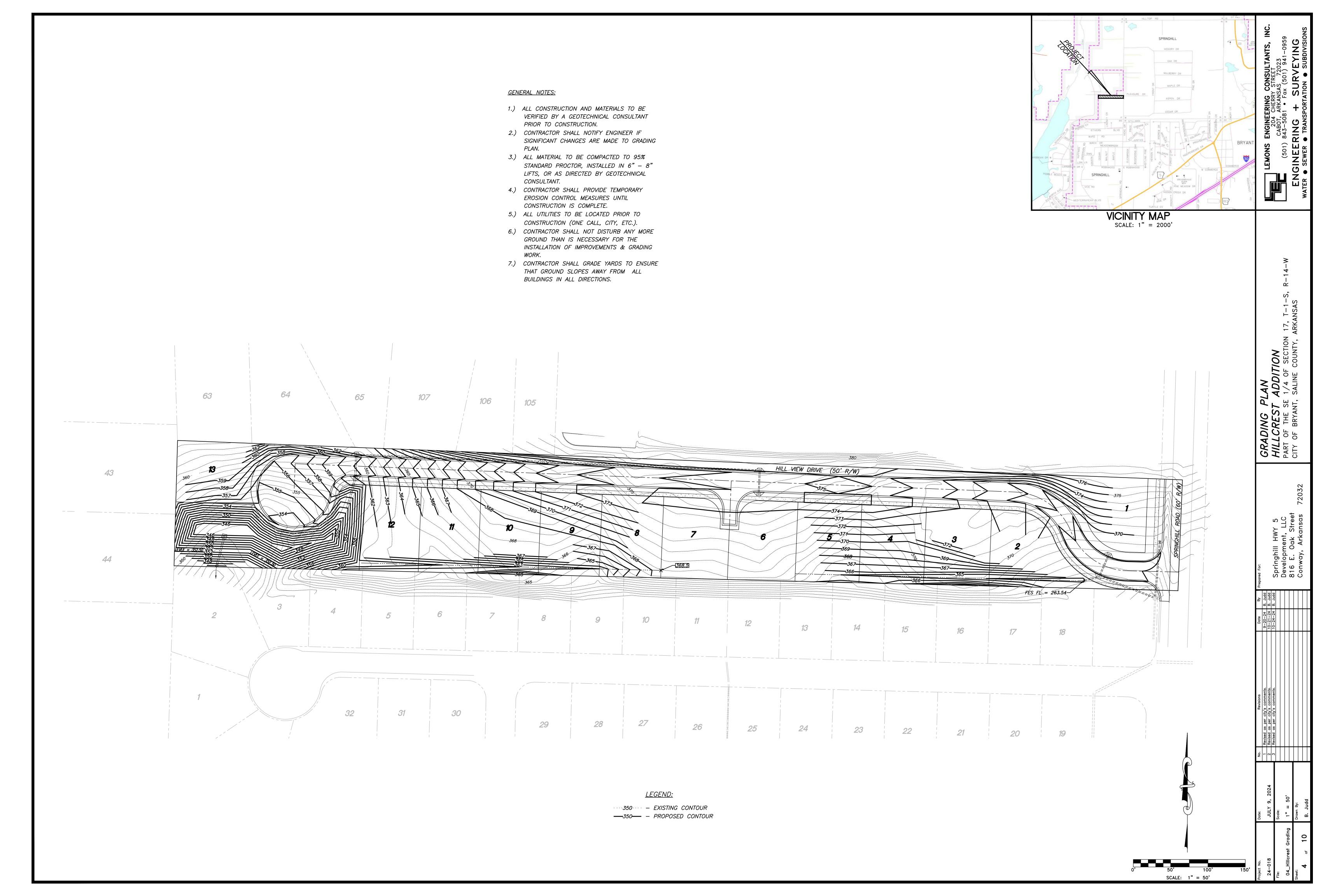




Revised as per city's comments.

10-21-24 B. Judd
Springhill HWY 5
Development, LLC
Brevelopment, LLC
Brevelopment, LLC
Conway, Arkansas 72032

ENGINEERING +



-----350 -- EXISTING CONTOUR **─**350**─** − PROPOSED CONTOUR CONC. RETAINING WALL  $\times$  76'
TOP = 363.00
BOTTOM (GRADE) = 360.00  $\setminus$ (SEE DETAILS) STA. 11+47 (RT)

CURB INLET # 7

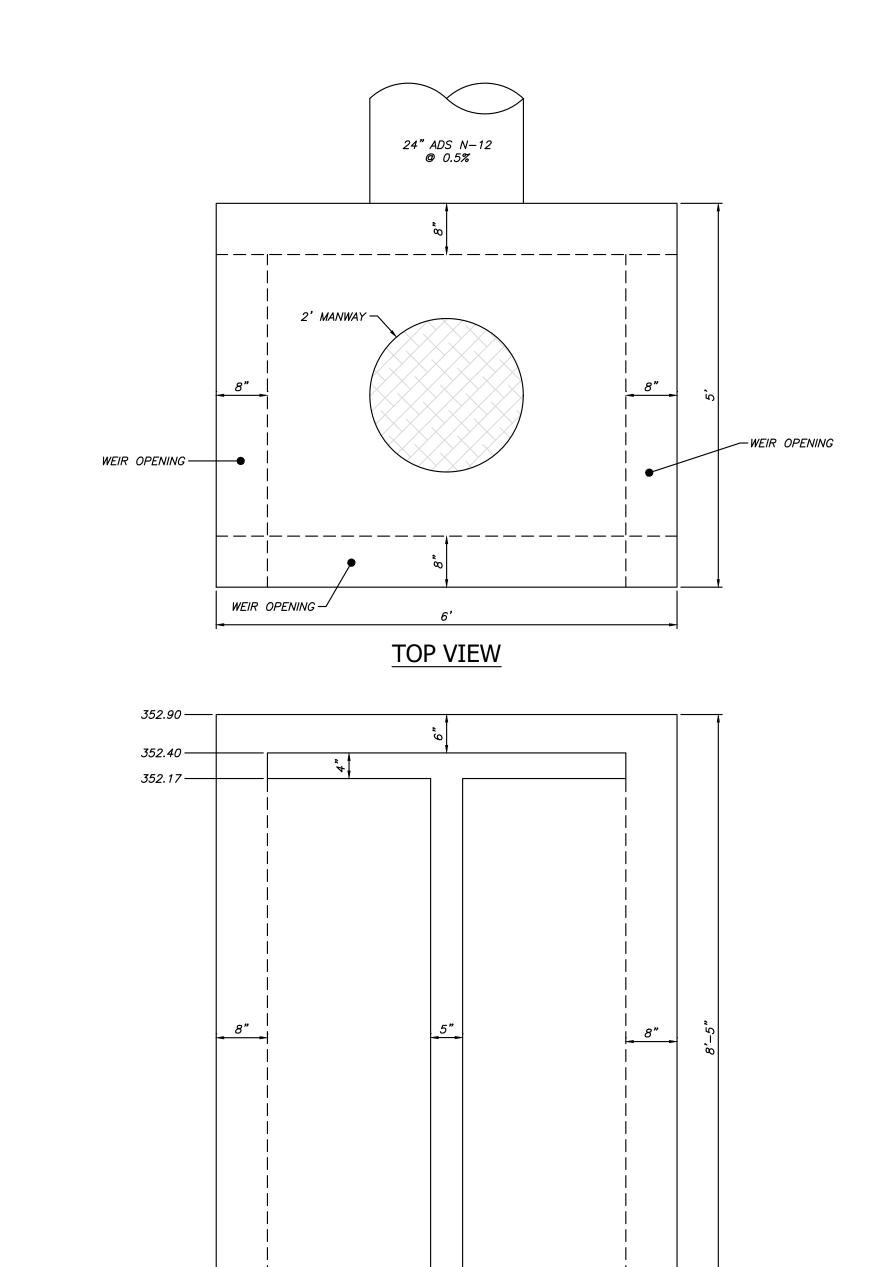
TOP = 361.21—

FL(18") = 356.77

FL(24") = 356.27 30' @ 2.0% 24" ADS N-12 x 100' @ 2.5% CONCRETE TRICKLE

CHANNEL x 35' @ 0.46% \_FES FL = 353.17 DET. DISCHARGE BOX \_ CONCRETE TRICKLE CHANNEL x 46' @ 12.33% LEVEE = 353.67 / -- 24" RCP @ 0.50% FL = 347.5FL = 345.61FL = 345.84\_CONCRETE TRICKLE CHANNEL x 66' @ 2.52% \_ CONCRETE TRICKLE CHANNEL x 52' @ 0.44% **GENERAL NOTES:** 1.) ALL CONSTRUCTION AND MATERIALS TO BE VERIFIED BY A GEOTECHNICAL CONSULTANT PRIOR TO CONSTRUCTION. 2.) CONTRACTOR SHALL NOTIFY ENGINEER IF SIGNIFICANT CHANGES ARE MADE TO GRADING \_ DISCHARGE BOX 3.) ALL MATERIAL TO BE COMPACTED TO 95%

<u>LEGEND:</u>



# DISCHARGE STRUCTURE NTS

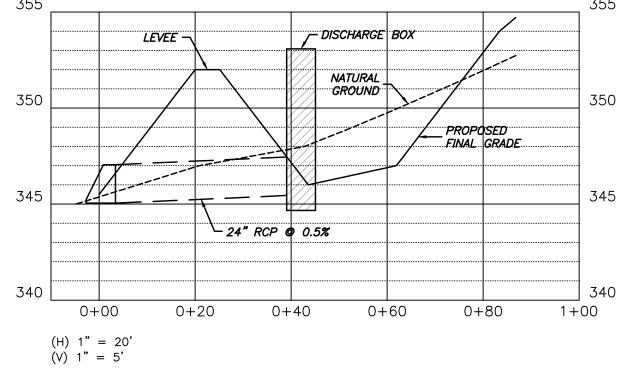
FRONT VIEW

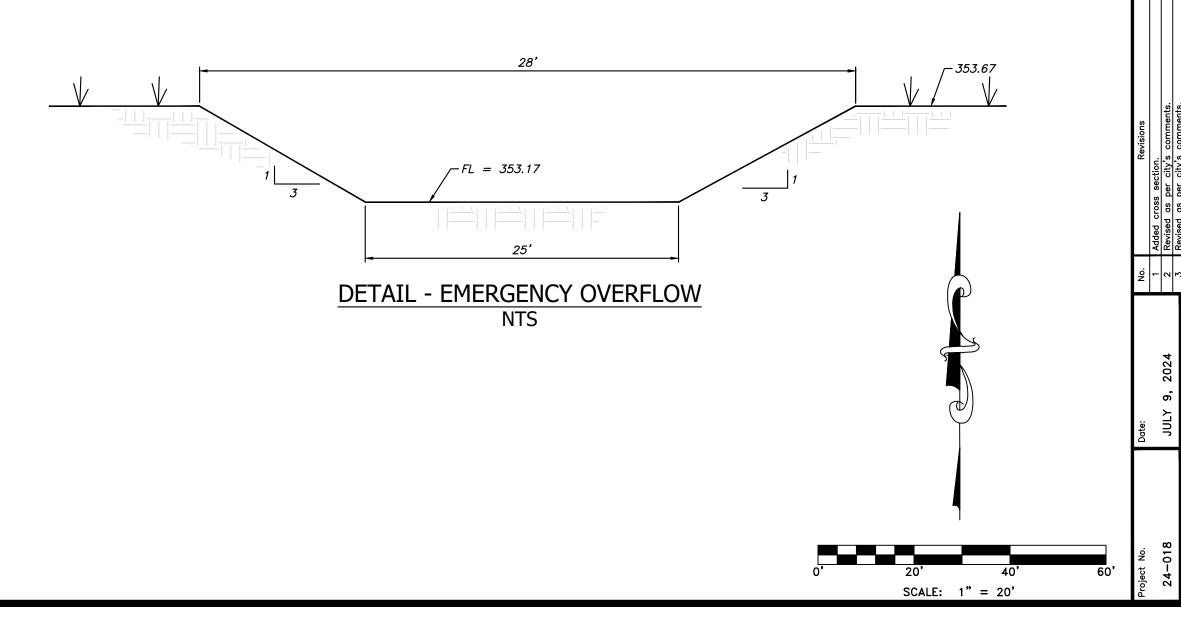
- 3.) ALL MATERIAL TO BE COMPACTED TO 95%

  STANDARD PROCTOR, INSTALLED IN 6" 8"

  LIFTS, OR AS DIRECTED BY GEOTECHNICAL

  CONSULTANT.
- 4.) CONTRACTOR SHALL PROVIDE TEMPORARY EROSION CONTROL MEASURES UNTIL CONSTRUCTION IS COMPLETE.
- 5.) ALL UTILITIES TO BE LOCATED PRIOR TO CONSTRUCTION (ONE CALL, CITY, ETC.).
- 6.) CONTRACTOR SHALL NOT DISTURB ANY MORE GROUND THAN IS NECESSARY FOR THE INSTALLATION OF IMPROVEMENTS & GRADING WORK.
- 7.) ALL LEVEES ASSOCIATED WITH DETENTION
  FACILITY SHALL NOT HAVE A SLOPE GREATER
  THAN 3:1.
- 8.) ALL AREAS OF DETENTION FACILITY SHALL INCLUDE SOLID SOD STABILIZATION.

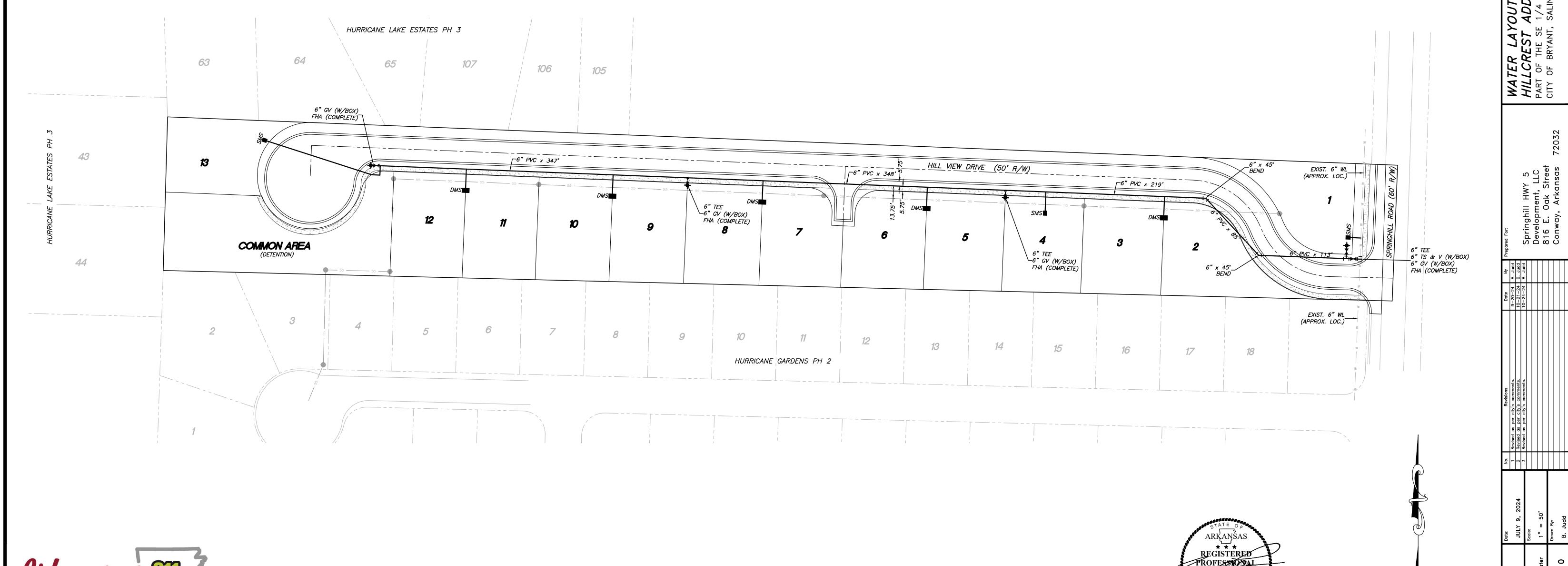




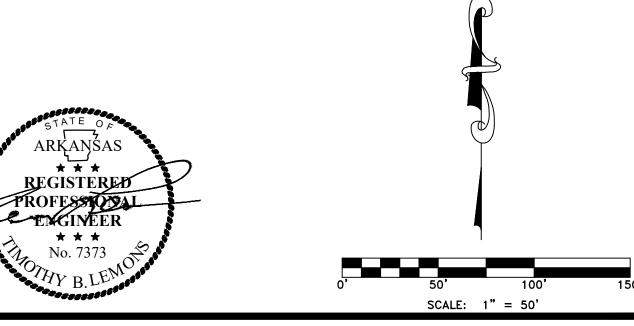


#### **GENERAL NOTES:**

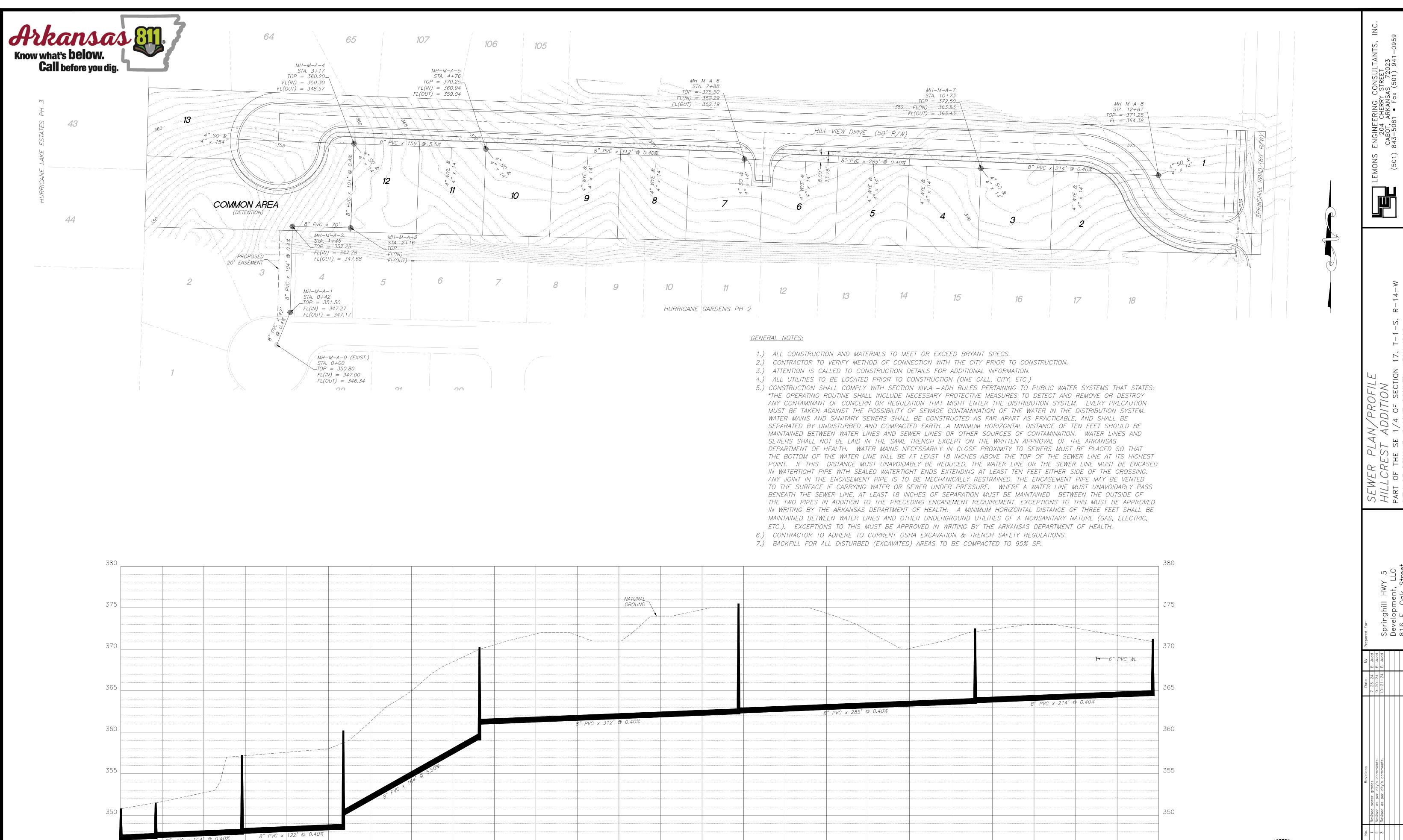
- 1.) ALL CONSTRUCTION AND MATERIALS TO MEET OR EXCEED SALEM WATER SPECIFICATIONS.
- 2.) INSTALL 12ga BLUE POLYETHELENE COATED SOLID COPPER WIRE IN A CONTINUOUS CIRCUIT UNDER ALL WATER MAINS AND SERVICE LINES. DIRECT BURY, WATERPROOF WIRE SPLICE CONNECTORS SHALL BE USED. TRACER WIRE SHALL BE TURNED UP AT ALL VALVES, HYDRANTS, METERS, AND BLOW-OFFS.
- 3.) ALL FITTINGS SHALL BE DUCTILE IRON M.J. (WHERE AVAILABLE).
- 4.) ATTENTION IS CALLED TO DETAILS FOR ADDITIONAL INFORMATION.
- 5.) CONSTRUCTION SHALL COMPLY WITH SECTION XIV.A ADH RULES PERTAINING TO PUBLIC WATER SYSTEMS THAT STATES: "THE OPERATING ROUTINE SHALL INCLUDE NECESSARY PROTECTIVE MEASURES TO DETECT AND REMOVE OR DESTROY ANY CONTAMINANT OF CONCERN OR REGULATION THAT MIGHT ENTER THE DISTRIBUTION SYSTEM. EVERY PRECAUTION MUST BE TAKEN AGAINST THE POSSIBILITY OF SEWAGE CONTAMINATION OF THE WATER IN THE DISTRIBUTION SYSTEM. WATER MAINS AND SANITARY SEWERS SHALL BE CONSTRUCTED AS FAR APART AS PRACTICABLE, AND SHALL BE SEPARATED BY UNDISTURBED AND COMPACTED EARTH. A MINIMUM HORIZONTAL DISTANCE OF TEN FEET SHOULD BE MAINTAINED BETWEEN WATER LINES AND SEWER LINES OR OTHER SOURCES OF CONTAMINATION. WATER LINES AND SEWERS SHALL NOT BE LAID IN THE SAME TRENCH EXCEPT ON THE WRITTEN APPROVAL OF THE ARKANSAS DEPARTMENT OF HEALTH. WATER MAINS NECESSARILY IN CLOSE PROXIMITY TO SEWERS MUST BE PLACED SO THAT THE BOTTOM OF THE WATER LINE WILL BE AT LEAST 18 INCHES ABOVE THE TOP OF THE SEWER LINE AT ITS HIGHEST POINT. IF THIS DISTANCE MUST UNAVOIDABLY BE REDUCED, THE WATER LINE OR THE SEWER LINE MUST BE ENCASED IN WATERTIGHT PIPE WITH SEALED WATERTIGHT ENDS EXTENDING AT LEAST TEN FEET EITHER SIDE OF THE CROSSING. ANY JOINT IN THE ENCASEMENT PIPE IS TO BE MECHANICALLY RESTRAINED. THE ENCASEMENT PIPE MAY BE VENTED TO THE SURFACE IF CARRYING WATER OR SEWER UNDER PRESSURE. WHERE A WATER LINE MUST UNAVOIDABLY PASS BENEATH THE SEWER LINE, AT LEAST 18 INCHES OF SEPARATION MUST BE MAINTAINED BETWEEN THE OUTSIDE OF THE TWO PIPES IN ADDITION TO THE PRECEDING ENCASEMENT REQUIREMENT. EXCEPTIONS TO THIS MUST BE APPROVED IN WRITING BY THE ARKANSAS DEPARTMENT OF HEALTH. A MINIMUM HORIZONTAL DISTANCE OF THREE FEET SHALL BE MAINTAINED BETWEEN WATER LINES AND OTHER UNDERGROUND UTILITIES OF A NONSANITARY NATURE (GAS, ELECTRIC, ETC.). EXCEPTIONS TO THIS MUST BE APPROVED IN WRITING BY THE ARKANSAS DEPARTMENT OF HEALTH.
- 6.) CONTRACTOR SHALL ADHERE TO CURRENT OSHA REGULATIONS FOR EXCAVATION & TRENCH SAFETY.
- 7.) CONTRACTOR TO ADHERE TO AWWA SPECS FOR BLOCKING.
- 8.) CONTRACTOR SHALL HAVE ALL UTILITIES LOCATED PRIOR TO CONSTRUCTION.
- 9.) CONTRACTOR SHALL CONTACT WATER & WASTEWATER UTILITIES FOR ALL APPLICABLE INSPECTION & TESTING.
- 10.) CONTRACTOR SHALL CONTACT WATER & WASTEWATER UTILITIES AT LEAST 24 HOURS PRIOR TO DISRUPTION OF ANY SERVICE.
- 11.) ALL MATERIALS AND COMPONENTS INSTALLED IN DRINKING WATER SYSTEMS ARE REQUIRED TO COMPLY WITH THE FEDERAL DEFINITION OF "LEAD FREE" CONTAINED IN PUBLIC LAW 111-380.







OUT ADDITION 1/4 OF SECTI SALINE COUNT



....@...0.40%....

(H) 1" = 50'(V) 1" = 5' 1 + 50

2+00

MH-M-F STA. 2+1 TOP = 2 FL(IN) = FL(OUT)

3+00

3+50

2+50

 $\begin{array}{r}
 M - A + 4 \\
 4 + 32 \\
 = 370... \\
 \sqrt{1} = 36 \\
 \sqrt{1} = 36
 \end{array}$ 

4+50

5+00

5+50

6+00

6+50

7+00

7+50

8+00

8+50

9+00

10+00

10 + 50

11+00

11 + 50

4+00

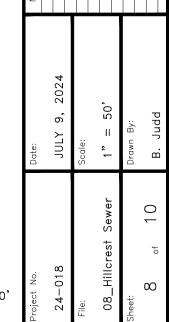
345

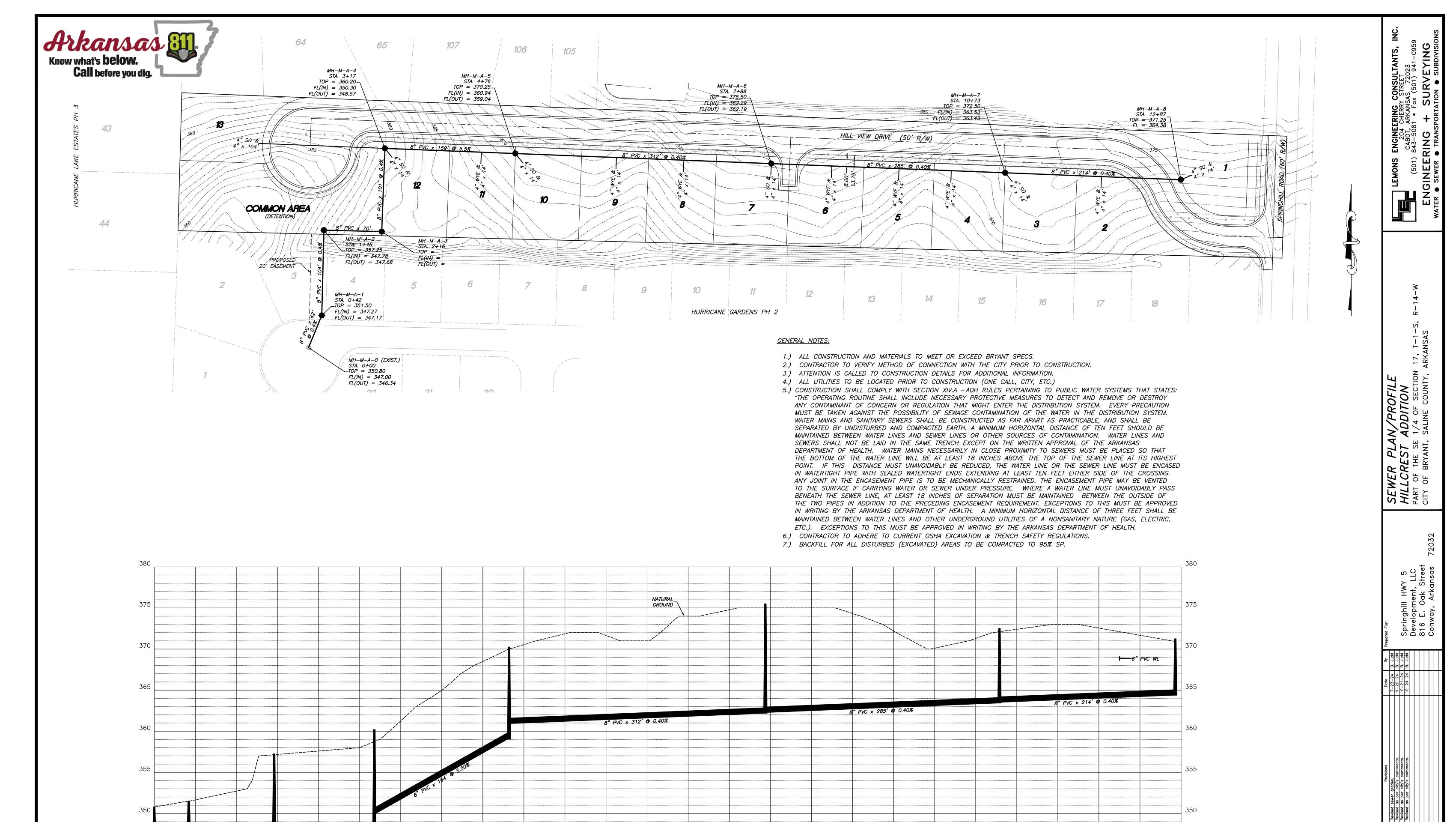


12+50

12+00

(H) 1" = 50'(V) 1" = 5'





8" PVC x 122' @ 0.40%

2+00

2+50

3+00

3+50

4+00

4+50

5+00

5+50

6+00

6+50

7+00

7+50

8+00

8+50

9+00

9+50

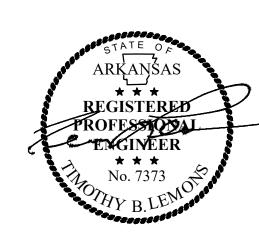
0+00

(H) 1" = 50' (V) 1" = 5'

0+50

1+00

1 + 50



350

#**\$6 2** 335

12+50

12+00

(H) 1" = 50'(V) 1" = 5'

MH-M-A-6 STA. 10+29 TOP = 372.50 FL(IN) = 363.5 FL(OUT) = 363.5

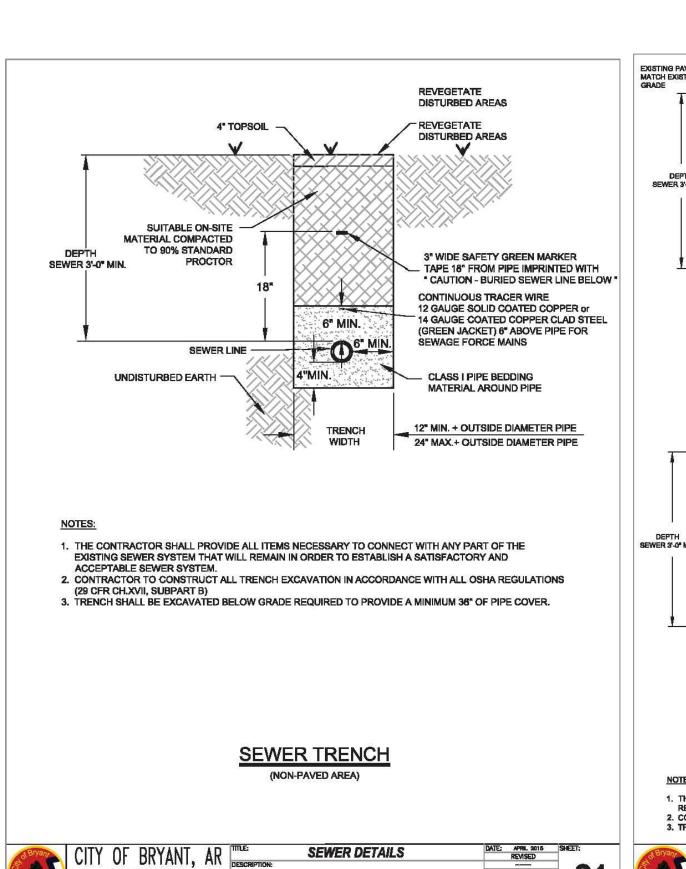
10+50

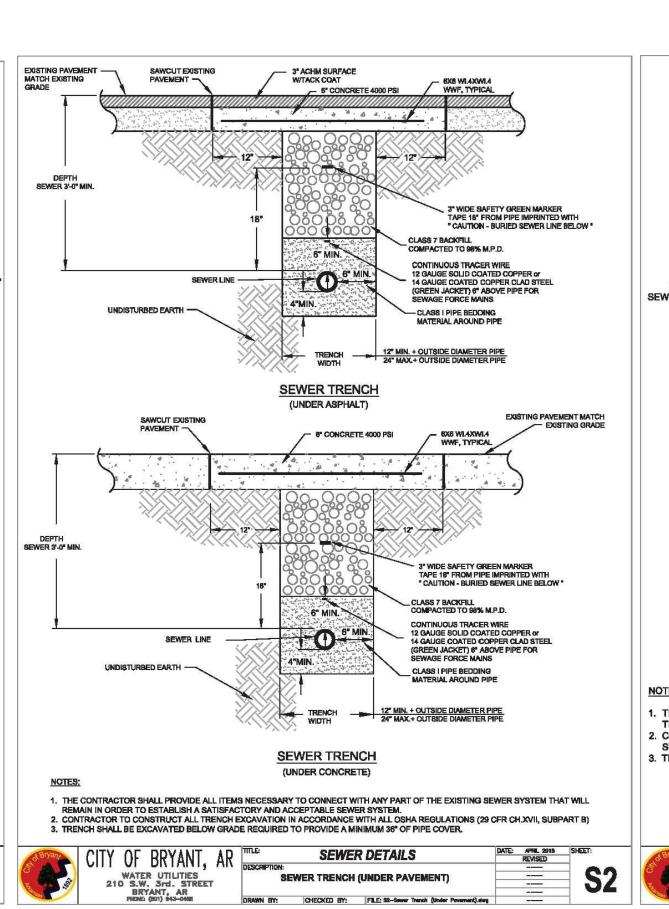
10+00

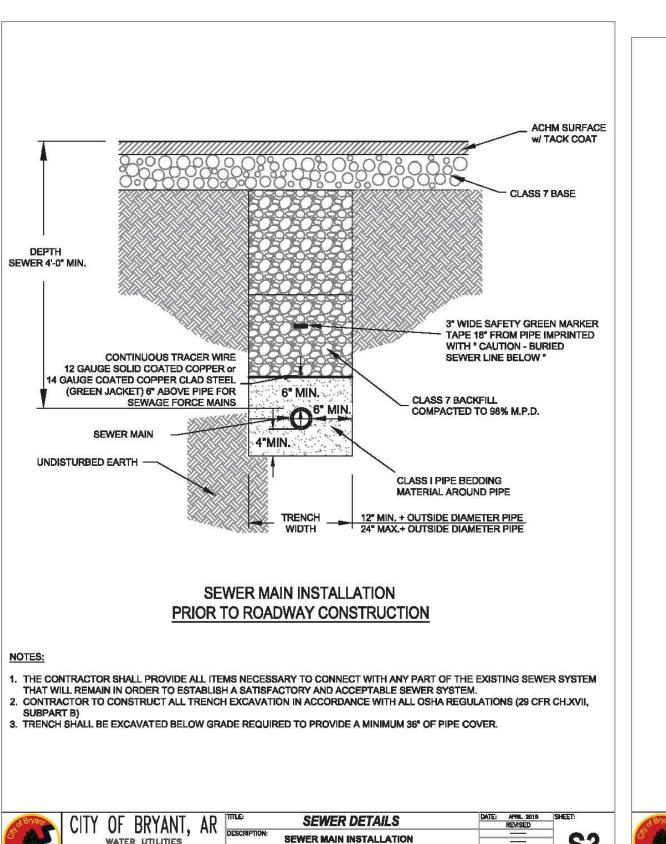
11+00

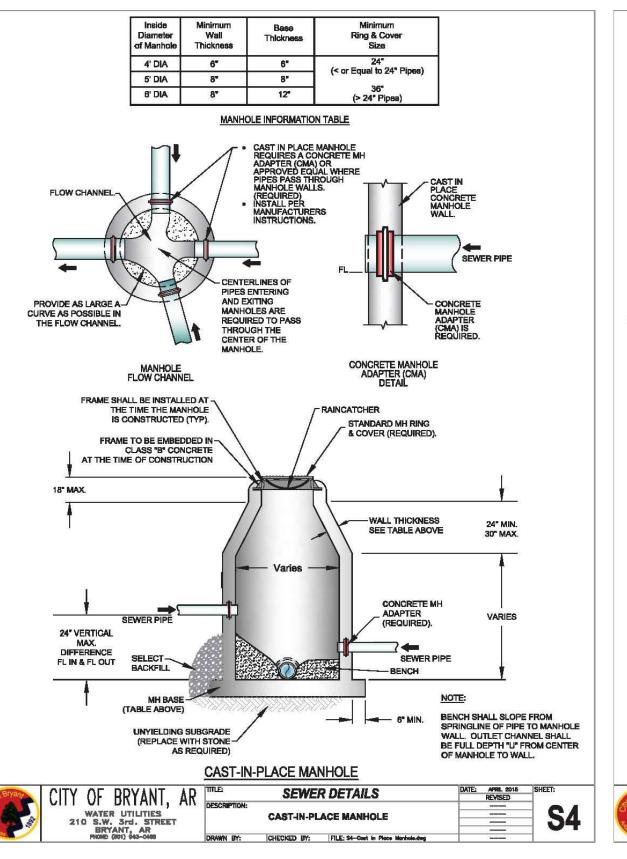
11+50

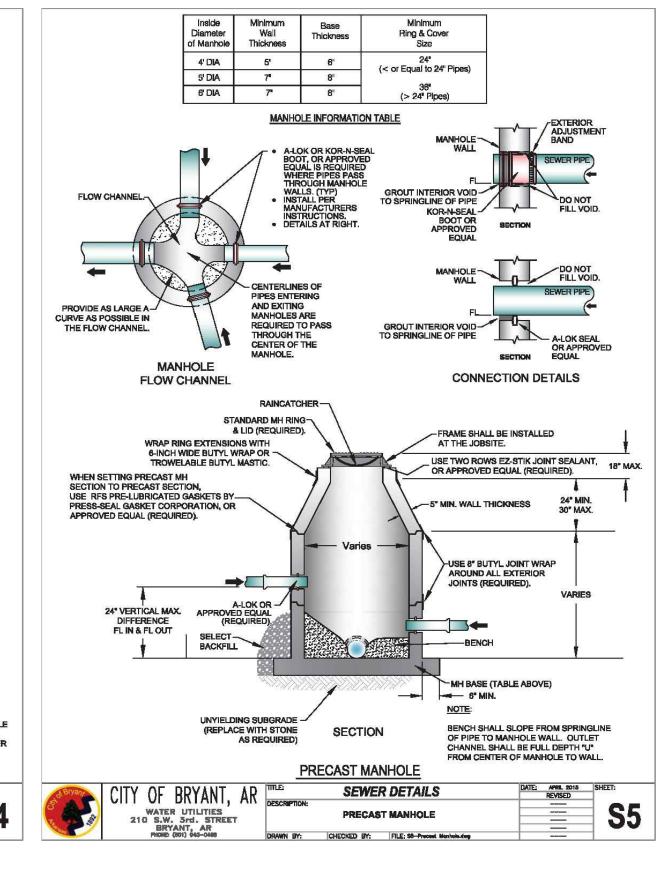
SCALE: 1" = 50'

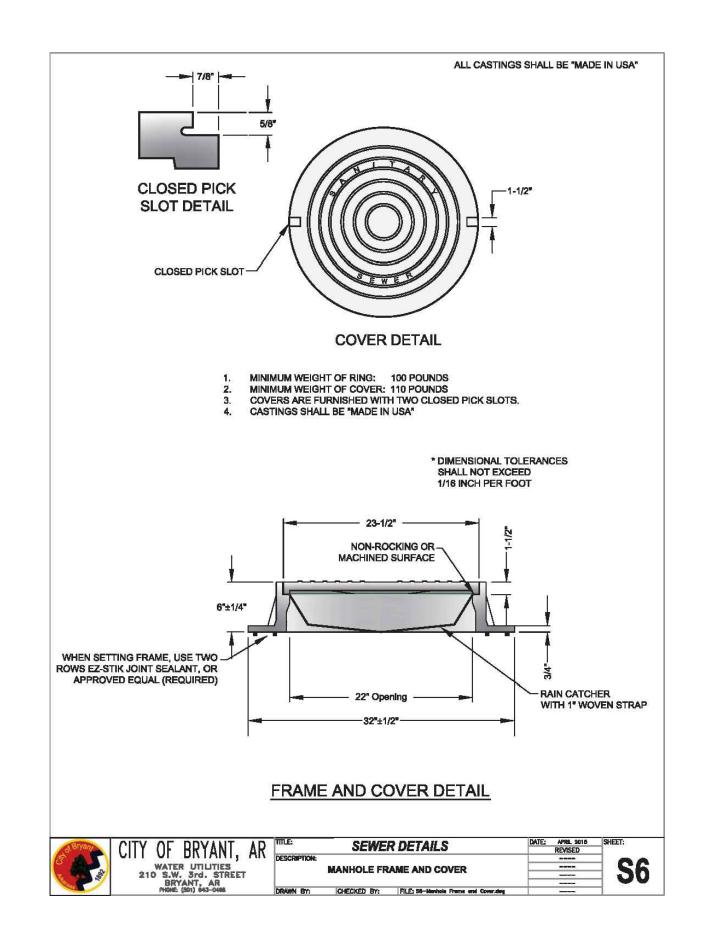


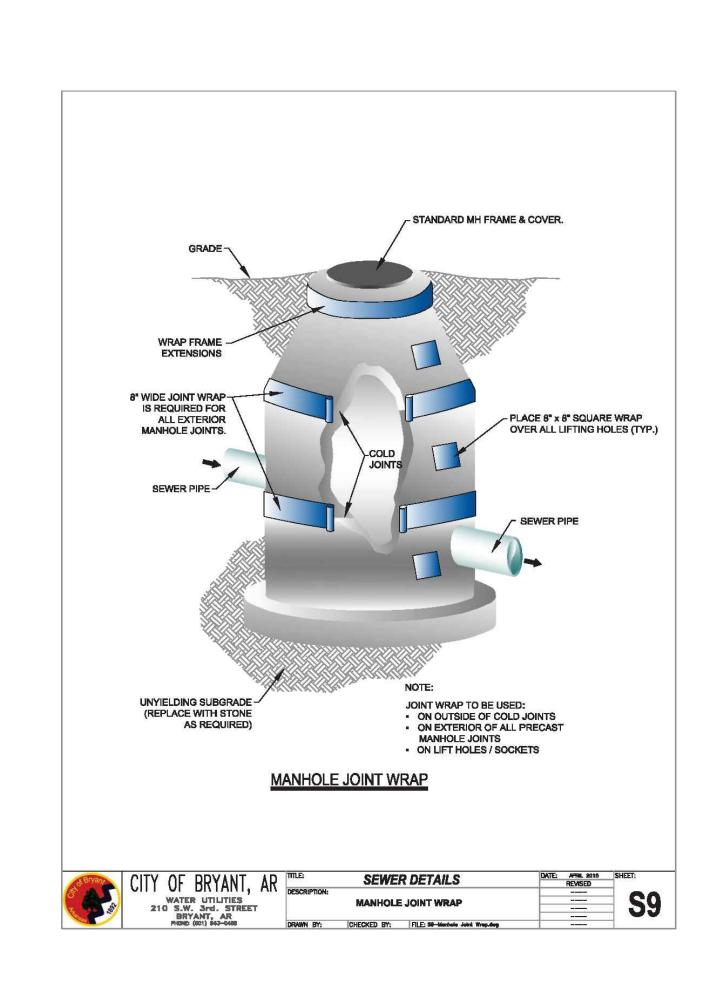


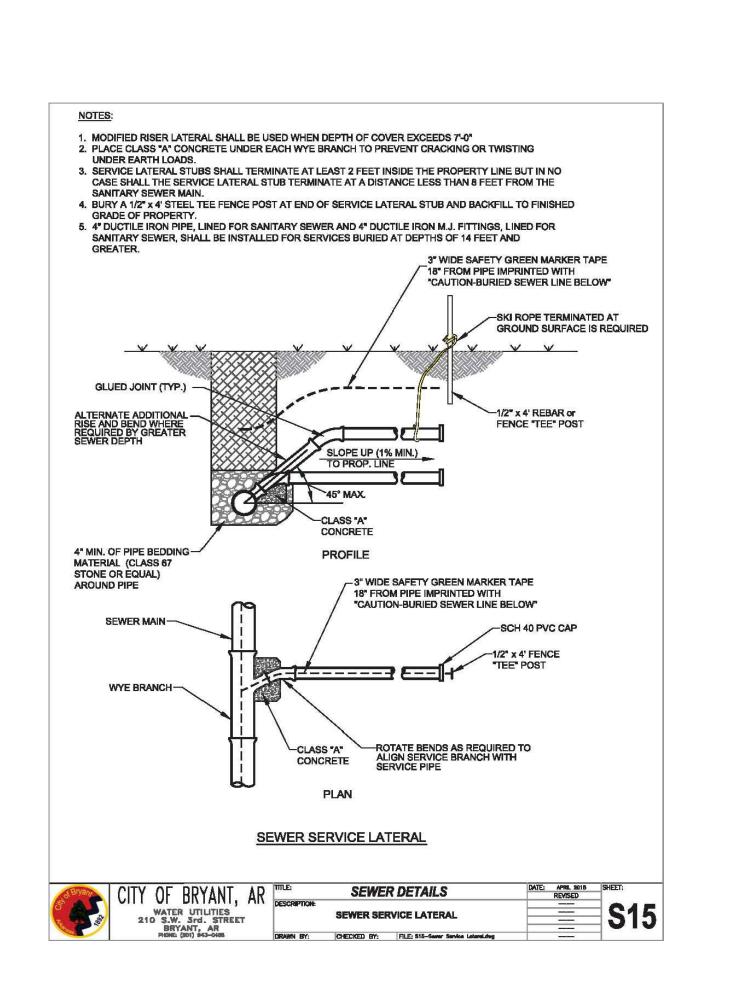


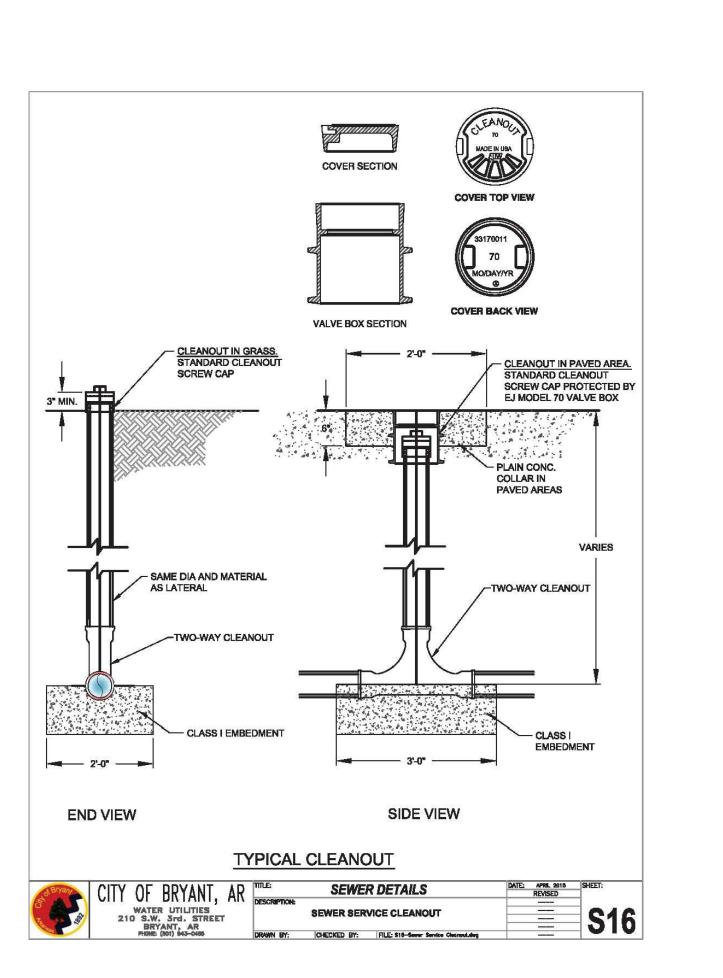












CONSTRI HILLCRE: PART OF THE CITY OF BRY											
Springhill HWY 5 Development, LLC 816 E. Oak Street Conway, Arkansas 72032											
By											
Date											
Revisions											
No.											
Date:	JULY 9, 2024	. 101 60 1100	Scale:		. N.⊤.S.		Drawn By:		מין. מ		
oject No.	24-018	0)	ie:		09 Hillcrest CD Sewer N.T.S.		leet:		ດ ອ້		

NEERING CONSULTANTS, II

10.4 CHERRY STREET

10.7 ARKANSAS 72023

10.8 5081 • Fax (501) 941-0959

10.8 CHERRY STREET

10.9 CHE

(C)

(50 **E** 

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#### **GENERAL NOTES:**

- 1.) A SILT FENCE AND STRAW BALE DIKE SHALL BE PLACED
  AT POTENTIAL LOCATIONS OF HEAVY EROSION.
- 2.) TEMPORARY STRAW BALE DIKES ARE TO BE CONSTRUCTED NOT TO POND WATER ON ADJACENT PROPERTY.
  3.) ALL TEMPORARY EROSION CONTROLS SHALL BE MAINTAINED
- UNTIL ALL CONSTRUCTION IS COMPLETE & PERMANENT
  GROUND COVER HAS BEEN ESTABLISHED.

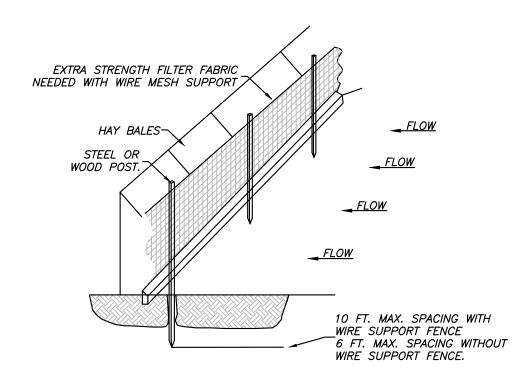
  4.) ONE OF THE FOLLOWING GROUND COVER METHODS SHALL
  BE USED AT ABEAS OF CLEARING OTHER THAN ELITIBE
- BE USED AT AREAS OF CLEARING OTHER THAN FUTURE
  PAVEMENT SURFACES:
  STRAW OR HAY-LOOSE
  2.0 TONS/ACRE
- STRAW ON HAT-LOOSE

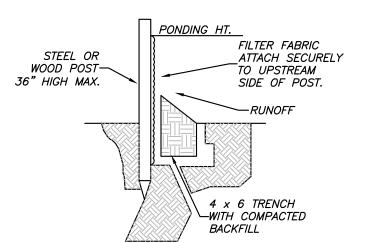
  STRAW OR HAY-TIED, ANCHORED, OR TACKED 1.5 TONS/ACRE

  5.) SOIL EXPOSED FOR MORE THAN 14 DAYS WITH NO
- CONSTRUCTION ACTIVITY SHALL BE SEEDED OR REVEGITATED.

  6.) CONSTRUCTION EXITS SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING ON FLOW OF MUD INTO PUBLIC RIGHT—OF—WAY.
- 7.) ADDITIONAL EROSION CONTROL MEASURES WILL BE EMPLOYED WHERE NECESSARY BY SITE CONDITIONS.
- 8.) CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING EROSION CONTROL MEASURES & PROVIDE RAIN FALL MONITORING & BI-WEEKLY INSPECTION REPORTS IN
- ACCORDANCE WITH THE NPDES PERMIT REQUIREMENTS.

  9.) CONTRACTOR SHALL USE "BEST MANAGEMENT PRACTICES"
  (BMP'S) WHEN IMPLEMENTING & MAINTAINING SEDIMENT & RUN-OFF CONTROLS.
- 10.) THE USE OF "BIO-DEGRADABLE SOCK" IS ALLOWED AS OPPOSED TO SILT FENCE.





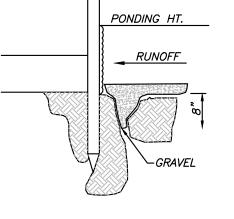


TRENCH WITH

NOTE:
1.) INSPECT AND REPAIR FENCE AFTER EACH
STORM EVENT AND REMOVE SEDIMENT WHEN
NECESSARY.

2.) REMOVED SEDIMENT SHALL BE DEPOSITED TO AN AREA THAT WILL NOT CONTRIBUTE SEDIMENT OFF—SITE AND CAN BE PERMANENTLY STABILIZED.

3.) SILT FENCE SHALL BE PLACED ON SLOPE CONTOURS TO MAXIMIZE PONDING EFFICIENCY.



ALTERNATE DETAIL TRENCH WITH GRAVEL

SILT FENCE

NTS

NOTES: 1.) PLACE CURB TYPE SEDIMENT BARRIERS ON GENTLY SLOPING STREET SEGMENTS WHERE WATER CAN POND AND ALLOW SEDIMENT TO SEPARATE FROM RUNOFF.

BACK OF SIDEWALK

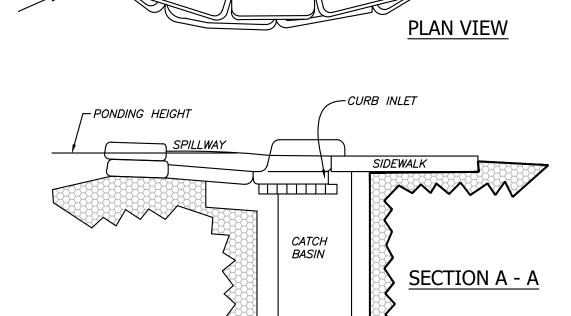
GRAVEL FILLED SANDBAGS

ARE STACKED TIGHTLY

2.) SANDBAGS OF EITHER BURLAP OR WOVEN GEOTEXTILE FABRIC ARE FILLED WITH GRAVEL, LAYERED, AND PACKED TIGHTLY.

3.) LEAVE ONE SANDBAG GAP IN THE TOP ROW TO PROVIDE A SPILLWAY FOR OVERFLOW.

4.) INSPECT BARRIERS AND REMOVE SEDIMENT AFTER EACH STORM EVENT. SEDIMENT AND GRAVEL MUST BE REMOVED FROM THE TRAVELED WAY IMMEDIATELY.

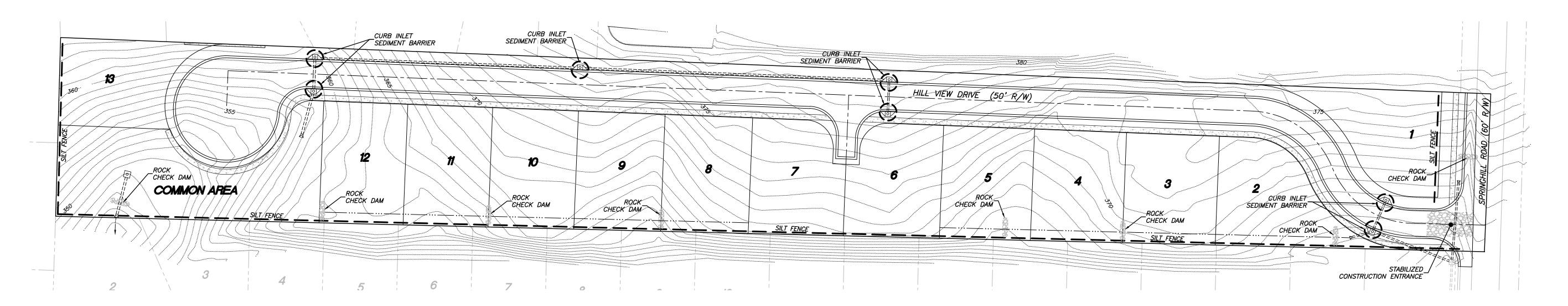


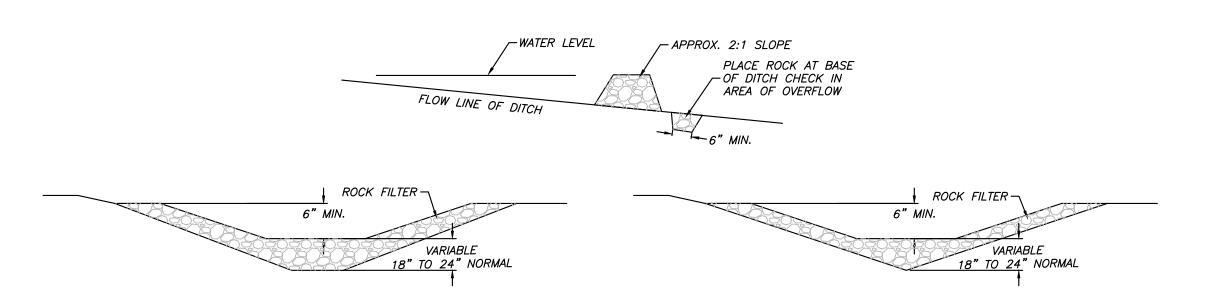
*⊢CATCH BASIN* 

\_CURB INLET

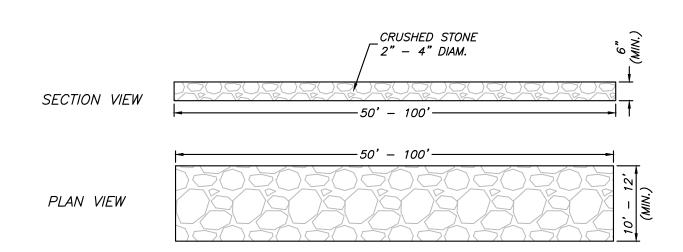
BACK OF CURB -

CURB INLET
SEDIMENT BARRIER



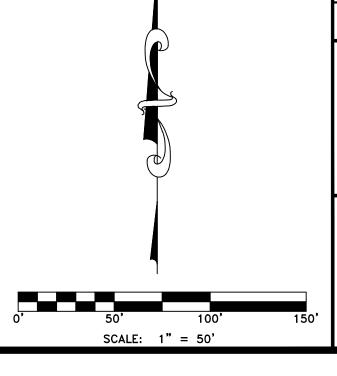


ROCK CHECK DAM NTS



STABILIZED CONSTRUCTION ENTRANCE NTS





No.

No.

Date:

No.

Revised as per city's con

JULY 9, 2024

2 Revised as per city's con

Scale:

Hillcrest Erosion

1" = 50\*

INEE



October 24, 2024

Mr. Colton Leonard, City Planner & Mr. Kelly Vanlandingham, PE, City Engineer City of Bryant, Arkansas Community Development 210 SW 3<sup>rd</sup> Street Bryant, Arkansas 72022

Re: Preliminary Plat

3927 Springhill Road, Bryant, AR

Parcel # 840-11855-000

Dear Mr. Leonard and Mr. Vanlandingham:

Please accept this letter in response to your latest comments as provided in an email on October 22. 2024. I will address the items in the order expressed (my response is shown in **bold italicized**):

#### **Drainage Calculations**

- The contours on the post construction drainage map (page 15) are so bold that I cannot read the inlet numbers or the flows. Not sure what the issue is on this matter. The separate pdf (large scale) that was a separate attachment shows up fine on our computers. I am resending it (full size).
- 2. At the bottom of page 20 Q bypass says 0% but it should be 32.6%. Whereas the amount of by pass is correct, I did not adjust the percentage. This typo has been corrected. The amount of by pass was included in the down stream inlet.
- 3. Page 33, show calculations for slotted weir. Is clogging included in the calculations? Yes. The vertical opening in the weir structure (below the 100 year storm elevation) is 2.78 sf. The horizontal opening on three sides of the box add 4.00 sf of opening, for a total of 6.78 sf. This is well more than what is needed for clogging.
- **4.** Page 34, detention pond calculations must show that post-construction flows from the pond are less than the pre-construction flows for 2, 5, 10, 25, 50, and 100 year storms (Section 1000.5.6, paragraph 2). **This is actually presented in the Summary-Detention Chart shown on Sheet 33.**

#### Drainage maps

- The post-construction map shows the discharge from Control Point A as being 12.88 cfs.
   Page 34 in the calculations shows it as being 16.81 cfs. This has been corrected. See attached revised map.
- The post-construction map shows discharge from Control Point B and C and there is no discharge shown in the calculations. This has been corrected. See attached revised map.
- 3. The post-construction map shows discharge from Control Point D as being 17.74 cfs but the calculations on page 34 show 38.08 cfs with no detention and 16.45 cfs with detention. *This has been corrected.* See attached revised map.

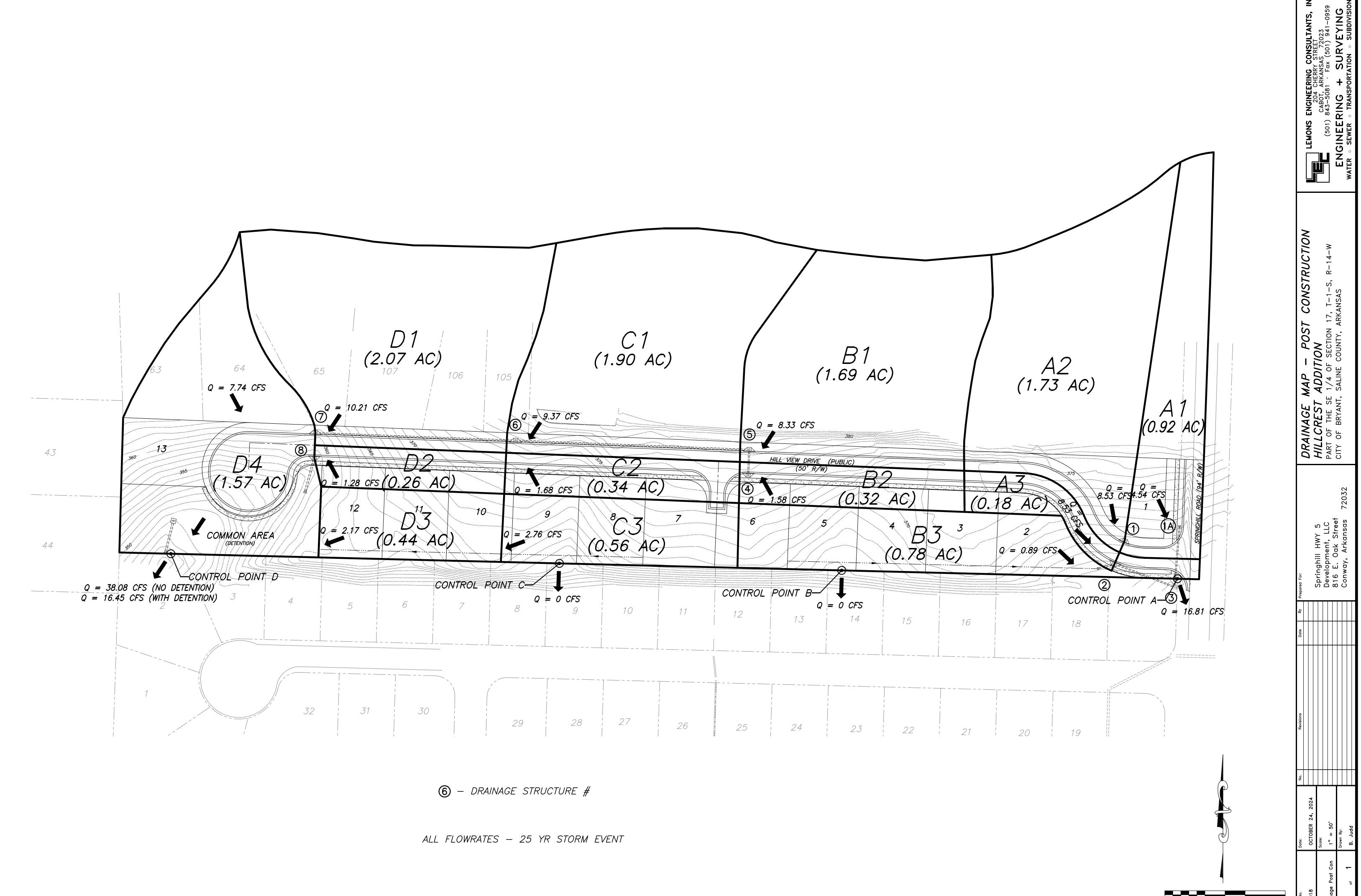
#### Construction Plans

- 1. Sheet 3 of 10 shows the existing 18" culvert stopping just behind the curb of the half-street improvements. Since the existing ditch will be graded over, it appears that this pipe should be extended to the north and pick up flow from the north. We will need to consult the owners as to when the half street improvements will be constructed. If the City and the Owner agree to an in leu of cost clause, the pipe will need to end in the vicinity of where it is shown on the existing plans. We are willing to discuss this with staff.
- 2. Sheet 3 of 10, show the existing ditch & culvert to the south of JB#3 along Springhill Road. Show details on how the outlet looks and how the flow will be handled to the south. We will be matching the existing half street road improvements from our planned intersection, to the South. This has been added to this sheet.
- 3. Sheet 5 of 10, show inlet numbers. Added as requested.
- **4.** Sheet 5 of 10, Is the top 4" slot all the way around the box beneath the top? **Yes. I have** added additional information on this detail to better represent this item.

Please let me know if you need anything additional.

Sincerely,

Tim Lemons, PE



# **Drainage Report**

For

# **Hillcrest Addition**

Springhill Road Bryant, Arkansas

Revised: October 24, 2024

### Prepared By:



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# **Project Information**

Project Title: Hillcrest Addition

**Project Description:** 13 lot single family development located on the West side of

Springhill Road, North of and adjacent to Hurricane Gardens,

Bryant, Arkansas (address: 3927 Springhill Road)

Owner/Developer: Springhill – Hwy 5 Development, LLC

816 East Oak Street

Conway, Arkansas 72032

**Engineer of Record:** Lemons Engineering Consultants, Inc.

Tim Lemons, PE 204 Cherry Street

Cabot, Arkansas 72023

(501) 605-7565

# **General Information**

This proposed development shall include 13 single family lots. This property is essentially the Northern Most tract of land within the city limits of Bryant as it presently exist. The property to the North of the subject site is developed with duplex style residential structures existing outside the City limits of Bryant. The property to the South is an established subdivision (Hurricane Gardens). The property drains North to South. There have been several reports of drainage issues by the residents of Hurricane Gardens. At present, the drainage from the subject property, and that to the north of the subject property, flows onto Hurricane Gardens. No detention exists on the property located north of the subject property.

#### The objectives of this report are as follows:

- Determine the estimated increase in runoff due to the development of Hillcrest Addition.
- 2) Provide design computations for a detention facility to bring the runoff from said tract to pre-construction rate.
- 3) Based on comments expressed by the residents, divert as much flow as possible away from the rear of the Northern most lots within Hurricane Gardens. As previously stated, the majority of the property to the North of Hurricane Gardens flows into the rear of the Northern most lots, creating an issue for the property owners.
- 4) Size the infrastructure in the development using the City's Drainage Code.
- 5) Compare the estimated Pre and Post flowrates at specific control points to show that the overall runoff from Hillcrest is at or less than the pre-construction flowrate.

The control points (A-D) to be used in this analysis are shown on the following vicinity map, and throughout this report.

# **Project Vicinity Map**



# **Hydrological Computations**

For this analysis, we will use the Rational Method in determining culvert sizes, culvert capacity computations, and other related issues on site. The total watershed size for this development is estimated at 12.40 acres. Attention is called to the Watershed Map included in this report. As per the Rational Method, the following equation is used:

Q = CxIxA, where:

Q = Flowrate (cfs)

C = Runoff Coefficient

I = Intensity (from tables)

A = area (acres)

The selection of the appropriate intensity is based on the estimated time of concentration (tc).

#### **Determination of Runoff Coefficients "C"**

In determining the Pre Construction C, we must consider the property to the North that is developed, and discharging onto the subject property. The C factor for Pre and Post Conditions are based on Table 400-1 "Runoff Coefficients for Surface Types" as provided in the Bryant Drainage Manual. A factored (weighted) value of C is determined in the following tables:

#### **Pre Construction Conditions**

Storm Event	Off Site	Off Site	Off Site	Off Site	On Site	On Site	On Site	On Site	Weighted
	C1	A1	C2	A2	C3	А3	C4	A4	С
		(acres)		(acres)		(acres)		(acres)	Factor
2	0.75	3.04	0.29	4.73	0.75	0.19	0.29	4.59	0.41
5	0.8	3.04	0.32	4.73	0.8	0.19	0.32	4.59	0.44
10	0.83	3.04	0.35	4.73	0.83	0.19	0.35	4.59	0.47
25	0.88	3.04	0.39	4.73	0.88	0.19	0.39	4.59	0.52
50	0.92	3.04	0.42	4.73	0.92	0.19	0.42	4.59	0.55
100	0.97	3.04	0.46	4.73	0.97	0.19	0.46	4.59	0.59

C1 (off site for homes, streets, etc.)

C2 (off site for grass, landscaping, etc.)

C3 (on site for homes, streets, etc.)

C4 (on site for grass. Landscaping, etc.)

A1 (off site area for C1)

A2 (off site area for C2)

A3 (on site area for C3)

A4 (on site area for C4)

#### **Post Construction Conditions**

Storm Event	Off Site	Off Site	Off Site	Off Site	On Site	On Site	On Site	On Site	Weighted
	C1	A1	C2	A2	C3	А3	C4	A4	С
		(acres)		(acres)		(acres)		(acres)	Factor
2	0.75	3.04	0.29	4.73	0.75	1.81	0.29	3.07	0.47
5	0.8	3.04	0.32	4.73	0.8	1.81	0.32	3.07	0.50
10	0.83	3.04	0.35	4.73	0.83	1.81	0.35	3.07	0.53
25	0.88	3.04	0.39	4.73	0.88	1.81	0.39	3.07	0.58
50	0.92	3.04	0.42	4.73	0.92	1.81	0.42	3.07	0.61
100	0.97	3.04	0.46	4.73	0.97	1.81	0.46	3.07	0.66

C1 (off site for homes, streets, etc.)

C2 (off site for grass, landscaping, etc.)

C3 (on site for homes, streets, etc.)

C4 (on site for grass. Landscaping, etc.)

A1 (off site area for C1)

A2 (off site area for C2)

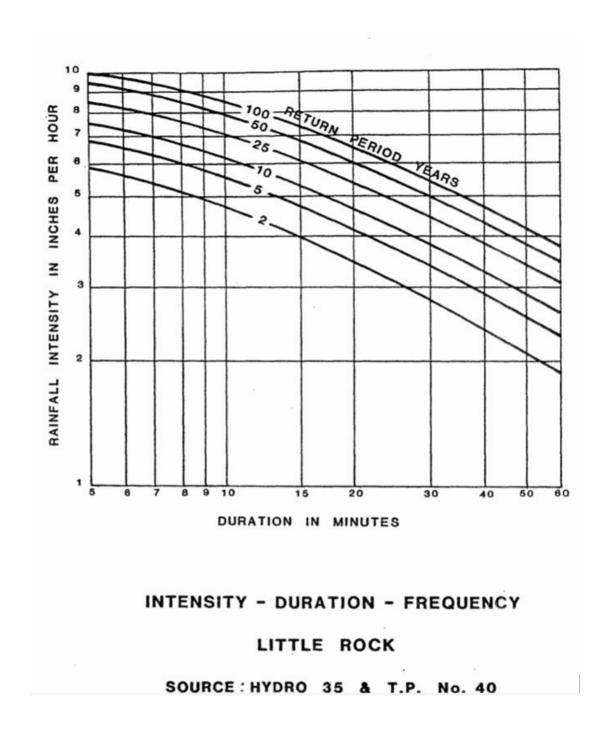
A3 (on site area for C3)

A4 (on site area for C4)

The above variable values will be used in designing the Detention Facility. For culvert design, we will use the Post C values for the 25 year storm.

### **Determination of Intensity Values "I"**

For this analysis, we will use the Intensity – Duration - Frequency Chart from the Little Rock Drainage Manual. Whereas the calculated value of I shall be used for Detention, we will use a tc (time of concentration) of 5 min for the culverts to also provide a conservative value.



# **Drainage Map (Pre-Construction)**



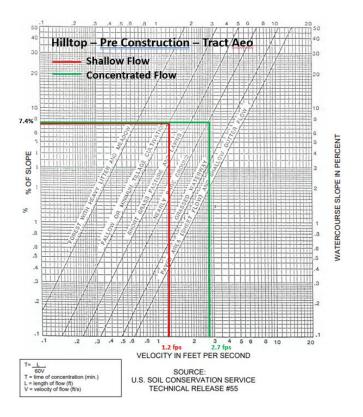
See attached map for additional information

### **Pre Construction Flowrates – Control Points**

The estimated Pre Construction Flowrate for each Control Point is estimated as follows. These values will be used to compare to the Post Construction Flowrate later in this report:

#### **Control Point A**

The time of concentration is determined as follows:



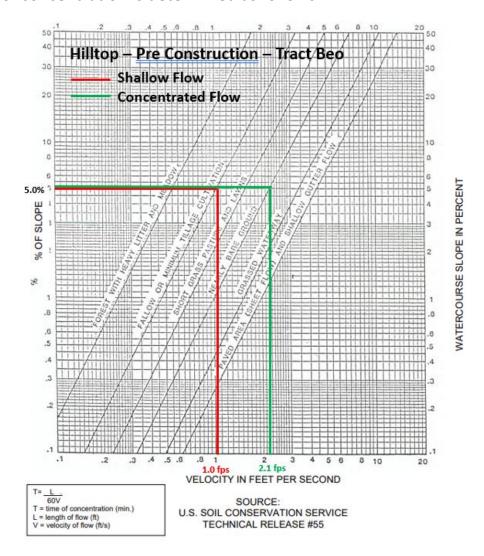
$$tc = ((300)/(60)(1.2)) + ((300)/(60)(2.7)) = 6 min$$

Flowrates for various Storm Events (Control Point A):

Storm Event	С	tc	I	Α	Q	
		(min)	(in/hour)	(acres)	(cfs)	
2	0.41	6	5.6	3.02	6.93	
5	0.44	6	6.6	3.02	8.77	
10	0.47	6	7.3	3.02	10.36	
25	0.52	6	8.2	3.02	12.88	
50	0.55	6	9.2	3.02	15.28	
100	0.59	6	9.8	3.02	17.46	

#### **Control Point B**

The time of concentration is determined as follows:



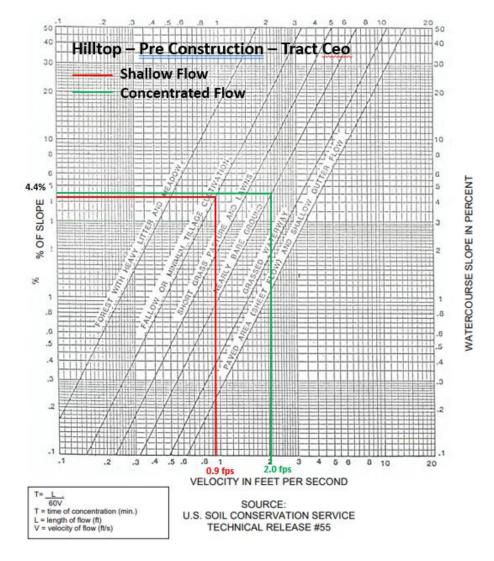
$$tc = ((300)/(60)(1.0)) + ((200)/(60)(2.1)) = 6.5 min$$

Flowrates for various Storm Events (Control Point B):

Storm Event	С	tc	ı	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	6.5	5.6	2.47	5.67
5	0.44	6.5	6.6	2.47	7.17
10	0.47	6.5	7.3	2.47	8.47
25	0.52	6.5	8.2	2.47	10.53
50	0.55	6.5	9.2	2.47	12.50
100	0.59	6.5	9.8	2.47	14.28

#### **Control Point C**

The time of concentration is determined as follows:



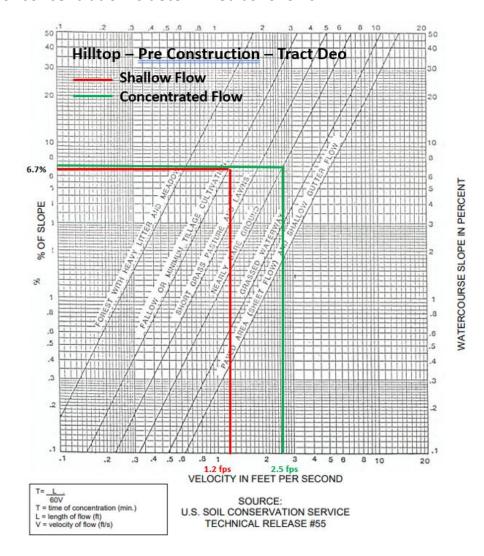
$$tc = ((300)/(60)(0.9)) + ((300)/(60)(2.0)) = 8 min$$

#### Flowrates for various Storm Events (Control Point C):

Storm Event	С	tc	I	Α	Q	
		(min)	(in/hour)	(acres)	(cfs)	
2	0.41	8	5.1	2.75	5.75	
5	0.44	8	6	2.75	7.26	
10	0.47	8	6.7	2.75	8.66	
25	0.52	8	7.7	2.75	11.01	
50	0.55	8	8.5	2.75	12.86	
100	0.59	8	9.1	2.75	14.76	

#### **Control Point D**

The time of concentration is determined as follows:



$$tc = ((300)/(60)(1.2)) + ((340)/(60)(2.5)) = 6.4 min$$

Flowrates for various Storm Events (Control Point D):

Storm Event	С	tc	I	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	6.5	5.6	4.16	9.55
5	0.44	6.5	6.6	4.16	12.08
10	0.47	6.5	7.3	4.16	14.27
25	0.52	6.5	8.2	4.16	17.74
50	0.55	6.5	9.2	4.16	21.05
100	0.59	6.5	9.8	4.16	24.05

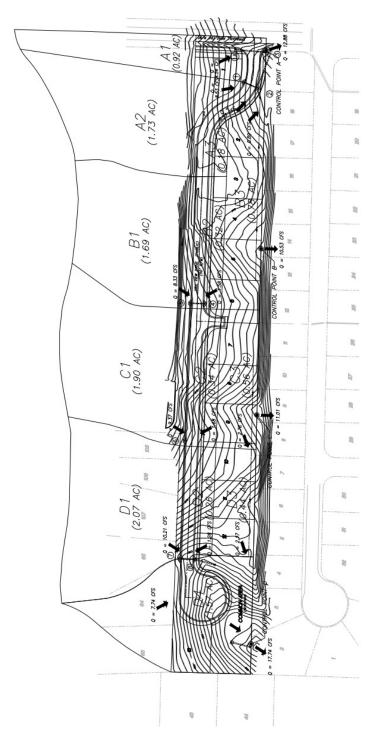
# **Determination of Flowrates for Culverts & Spreadflow**

Attention is called to the following chart which provides C, Intensity, Area, and Flowrate (Q) of each Tract. Again, the Rational Method is being used for all basins. Attention is called to the Maps on the next two pages for a detailed drawings showing the various watershed tracts. The 25 year storm event will be used for culvert design. A conservative tc of 5 minutes is used for the culvert design.

Tract	C(Post)	125	Α	Q25
		(in/hr)	(ac)	(cfs)
A1	0.58	8.5	0.92	4.54
A2	0.58	8.5	1.73	8.53
A3	0.58	8.5	0.18	0.89
B1	0.58	8.5	1.69	8.33
B2	0.58	8.5	0.32	1.58
В3	0.58	8.5	0.78	3.85
C1	0.58	8.5	1.90	9.37
C2	0.58	8.5	0.34	1.68
C3	0.58	8.5	0.56	2.76
D1	0.58	8.5	2.07	10.21
D2	0.58	8.5	0.26	1.28
D3	0.58	8.5	0.44	2.17
D4	0.58	8.5	1.57	7.74

# **Drainage Map (Post Construction)**

#### Revised 10/21/2024



See attached Map for additional information

# **Culvert Sizing**

All culverts are sized to meet a 25 year storm, and the Rational Method is used. We will use a Manning's Coefficient of 0.012 shall be for all culverts (concrete and HDPE). The d/D ratio and velocity was computed using HawsEDC On-Line Calculator (hawsedc.com).

#### FES 1a

Q = Qa1 = 4.54 cfs Use 18" @ 3.5% Q capacity = 21.94 cfs V actual = 9.68 fps (d/D = 0.32)

#### Inlet 1

Q = Qa2 = 8.53 cfs Use 18" @ 1.1% Q capacity = 12.30 cfs V actual = 7.36 fps (d/D = 0.63)

#### Inlet 2

Q = Inlet 1 + Qa3 = 8.53 + 0.89 = 9.42 cfs Use 24" @ 0.3% Q capacity = 13.84 cfs V actual = 4.63 fps (d/D = 0.62)

#### Junction Box 3 (verify capacity)

Q = Inlet 2 + Qb3 + Exist 18" in Hurricane Gardens (Culvert in Hurricane Gardens is an 18" ADS at 0.46%, Capacity = 7.95 cfs at d/D=0.85) Q = 9.42 + 3.85 + 7.95 = 21.22 cfs Existing 24" Discharging from Junc Box is 24" ADS @ 5.20% Q capacity = 57.58 cfs **Capacity appears to exist** V actual = 16.61 fps (d/D = 0.43)

#### Inlet 4

Q = Qb2 = 1.58 cfs Use 18" @ 0.5% Q capacity = 8.29 cfs V actual = 3.53 fps (d/D = 0.30)

#### Inlet 5

Q = Inlet 4 + Qb1 = 1.58 + 8.33 = 9.91 cfs Use 18" @ 1.0% Q capacity = 11.73 cfs V actual = 7.25 fps (d/D = 0.72)

#### Inlet 6

Q = Inlet 5 + Qc1 = 9.91 + 9.37 = 19.28 cfs Use 18" @ 4.60% Q capacity = 25.15 cfs V actual = 15.30 fps (d/D = 0.67)

#### Inlet 7

Q = Inlet 6 + Qd1 = 19.28 + 10.21 = 29.49 cfs Use 24'' @ 2.0%Q capacity = 35.71 cfs V actual = 12.38 fps (d/D = 0.71)

#### Inlet 8

Q = Inlet 7 + Qc2 + Qd2 = 29.49 + 1.68 + 1.28 = 32.45 cfs Use 24" @ 2.25% Q capacity = 37.87 cfs V actual = 13.28 fps (d/D = 0.73)

# **Street Spreadflow Analysis & Inlet Capture**

In this Section of the Report, we will examine how the stormwater in the street gutters may impact in proposed inlets. We will use our 27' street width (back of curb to back of curb), while giving allowances for the vertical portion of the curb on each side. The crown on the street shall be 3.0%. The available street width, to handle the stormwater, has a width of 26'. Our goal is to provide a minimum "non submerged" street width ("clear space") of 8 feet. We will use the following equation (as provided in "Urban Drainage and Flood Control District – Urban

Storm Drainage Manual, Volume 1, dated January, 2016) to determine the required length of throat to capture 100% of the stormwater:

```
Lt = 0.38 (Q^0.51)(SI^0.058)(1/nSx)^0.46, where:

Lt = required length of throat to capture 100%

Q = flowrate (cfs)

SI = slope of gutter

N = manning's coef. = 0.012

Sx = cross slope of street = 0.03
```

Since n and Sx are constant, the equation can be reduced to:

```
Lt = 0.38 (Q^0.51)(SI^0.058)(38.38)
Lt = 14.58 (Q^0.51) (SI^0.058)
```

Attention is called to the Appendix for the spreadsheets used to evaluate these areas.

#### Check Inlet 1 & 2 – Hillcrest Drive (Spreadflow Analysis)

#### Inlet 1

Q = Qa2 = 8.53 cfs

Gutter Slope = 1.50%Height of water (from gutter) = 0.33'Width of water (from gutter) = 11.0'Clear space (half street) = 13.0 - 11.0' = 2.0'Inlet 2 Q = Qa3 = 0.89 cfs Gutter Slope = 1.50%Height of water (from gutter) = 0.14'Width of water (from gutter) = 4.5'Clear space (half street) = 13.0 - 4.5' = 8.5'Total Clear Space = 2.0 + 8.5 = 10.5'

#### Stormwater Capture - Inlet 1

Lt = 14.58 (8.53^0.51)(0.015^0.058) = 34.10 feet Using a 20' throat: Q captured = 5.01 cfs (58.7%) Q bypass = 3.52 cfs (41.3%)

#### **Stormwater Capture – Inlet 2**

Lt = 14.58 (0.89^0.51)(0.015^0.058) = 10.77 feet Using a 12' throat: Q captured = 0.89 cfs (100%) Q bypass = 0.00 cfs (0%)

#### Check Inlet 4 & 5 – Hillcrest Drive (Spreadflow Analysis)

#### Inlet 4

Q = Qb2 = 1.58 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.21'

Width of water (from gutter) = 7.0'

Clear space (half street) = 13.0 - 7.0 = 6.0'

#### Inlet 5

Q = Qb1 = 8.33 fps

Gutter Slope = 0.5%

Height of water (from gutter) = 0.39'

Width of water (from gutter) = 13.0'

Clear space (half street) = 13.0 - 13.0' = 0.0'

Total Clear Space = 6.0 + 0.0 = 6.0

#### **TRY 10 YEAR STORM**

#### Inlet 4

Q = Qb2 = 1.26 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.20'

Width of water (from gutter) = 6.5'

Clear space (half street) = 13.0 - 6.5' = 6.5'

#### Inlet 5

Q = Qb1 = 6.66 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.36'

Width of water (from gutter) = 12.0'

Clear space (half street) = 13.0 - 12.0' = 1.0'

Total Clear Space = 6.5 + 1.0 = 7.5'

#### Stormwater Capture - Inlet 4

Lt =  $14.58 (1.26^{0.51})(0.005^{0.058}) = 12.06$  feet

Using a 13' throat:

Q captured = 1.26 cfs (100%)

Q bypass = 0.00 cfs (0%)

#### Stormwater Capture – Inlet 5

Lt = 14.58 (6.66^0.51)(0.005^0.058) = 28.20 feet

Using a 24' throat:

Q captured = 5.67 cfs (85.1%)

Q bypass = 0.99 cfs (14.9%)

# Check Inlet 6 & Across Street - Hillcrest Drive (Spreadflow Analysis) Inlet 6

Q = Qc1 = 9.37 cfs

Gutter Slope = 2.67%

Height of water (from gutter) = 0.30'

Width of water (from gutter) = 10.0'

Clear space (half street) = 13.0 - 10.0' = 3.0'

#### **Across from Inlet 6**

Q = Qc2 = 1.68 cfs

Gutter Slope = 2.67%

Height of water (from gutter) = 0.17'

Width of water (from gutter) = 5.5'

Clear space (half street) = 13.0 - 5.5 = 7.5

Total Clear Space = 3.0 + 7.5 = 10.5'

#### Stormwater Capture - Inlet 6

Q = 9.37 + 0.99 (bypass from Inlet 5) = 10.36 cfs

Lt = 14.58 (10.36^0.51)(0.0267^0.058) = 38.93 feet

Using a 30' throat:

Q captured = 7.99 cfs (77.1%)

Q bypass = 2.37 cfs (22.9%)

#### Check Inlet 7 & 8 - Hillcrest (Spreadflow Analysis)

#### Inlet 7

Q = Qd1 = 10.21 cfs

Gutter Slope = 4.88%

Height of water (from gutter) = 0.29'

Width of water (from gutter) = 9.5'

Clear space (half street) = 13.0 - 9.5' = 2.5'

#### Inlet 8

Q = Qc2 + Qd2 = 2.42 + 2.17 = 2.96 cfs

Gutter Slope = 4.88%

Height of water (from gutter) = 0.18'

Width of water (from gutter) = 6.0'

Clear space (half street) = 13.0 - 6.0' = 7.0'

Total Clear Space = 2.5 + 7.0 = 9.5

#### Stormwater Capture – Inlet 7

Q = 10.21 + 2.37 (bypass from Inlet 6) = 12.58 cfs

Lt = 14.58 (12.58^0.51)(0.0488^0.058) = 44.5 feet

Using a 30' throat:

Q captured = 8.48 cfs (67.4%)

Q bypass = 4.10 cfs (32.6%)

#### **Stormwater Capture – Inlet 8**

Lt = 14.58 (2.96^0.51)(0.0488^0.058) = 21.28 feet Using a 22' throat: Q captured = 21.28 cfs (100%) Q bypass = 0.00 cfs (0%)

#### **Curb Cut on Street at North side of Detention Pond**

Q = Qd4 + 4.10 (bypass from Inlet 7) = 7.74 + 4.10 = 11.84 cfs Use a 6" x 8' Curb Cut with a slope of 3%: Q =  $(1.49/n)(A)(R^2/3)(S^1/2) = (1.49/0.012)(4)(4.33)(0.17) = 22.44$  cfs

# **Detention Facility Computations**

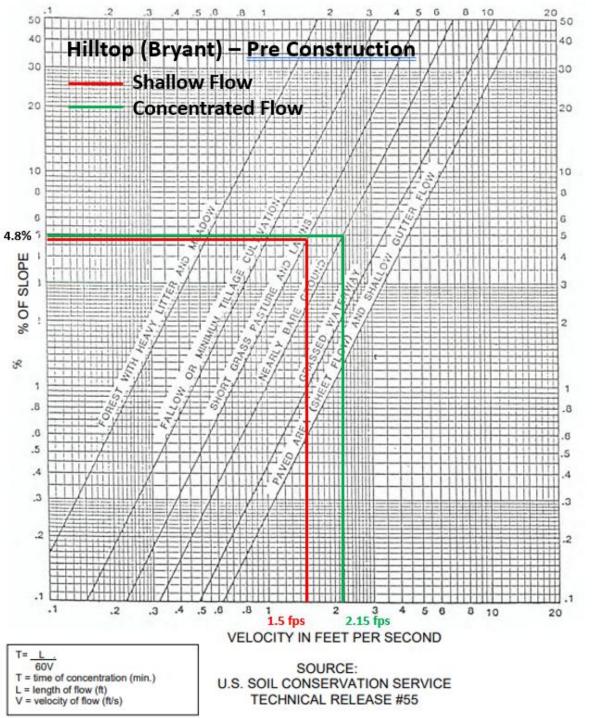
In this section, we will size the detention facility located in the Common Area (West side of the project). At the completion of this section, a summary of pre and post flows will be provided. Whereas the time of concentration will be used to determine the intensity (I), the runoff coefficient (C) for each storm analysis shall be based on that determined on pages 5 and 6 of this report.

# Time of Concentration (tc)

In determining the time of concentration, we must first determine the velocity of the runoff based on the type of ground cover and type of flow. The total tc is a sum of the tc for overland flow, the tc for shallow concentrated flow, and the tc for channelized flow. For this analysis, we will use the US Soil Conservation Service Technical Release #55, "Watercourse Slope vs Velocity" graph. A Pre Construction and Post Construction graph for each watershed is provided on the following pages.

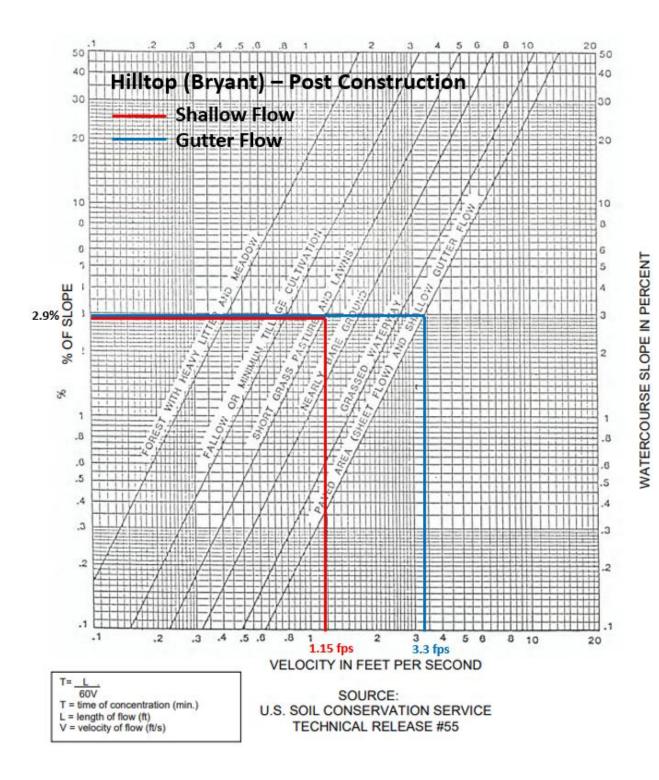
# WATERCOURSE SLOPE IN PERCENT

# **Pre Construction Time of Concentration (tc)**



Pre-Construction tc =  $\Sigma(L/(60)(V))$  = 6 min

# **Post Construction Time of Concentration (tc)**



Post-Construction tc =  $\Sigma(L/(60)(V))$  = 9 min

## **Stage – Storage Table**

The following Stage Storage Table is provided, based on the grading plan contained in the Civil Plans. The accumulative storage is provided in the right most column.

TYPE 3									
Stage - Storage for Irregular Detention Basin									
Top Elev	Bottom Elev	Increment							
353.5	345.5	1							
Stage	Area	Δ Volume	Volume						
msl	sf	cf	cf						
345.50	1	0	0						
346.50	1853.50	927.25	927.25						
347.50	2951.40	2402.45	3329.70						
348.50	4240.13	3595.77	6925.47						
349.50	5637.46	4938.80	11864.26						
350.50	7118.75	6378.11	18242.37						
351.50	8673.71	7896.23	26138.60						
352.50	10265.99	9469.85	35608.45						
353.50	11858.27	11062.13	46670.58						

# Stage - Discharge Table

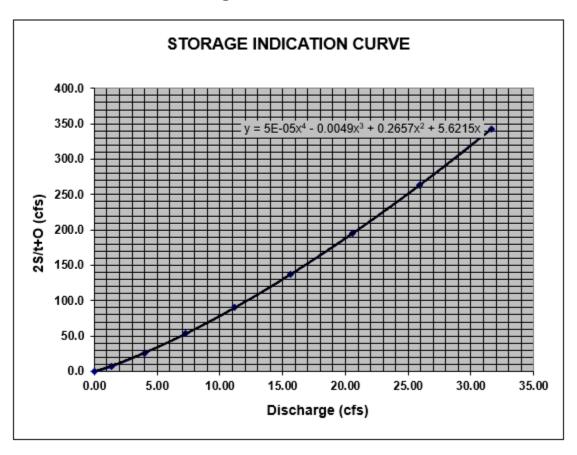
The following Stage Discharge Table is provided, based on the grading plan contained in the Civil Plans. The discharge structure planned for this facility is shown later in this report.

TYPE 2

Stage - Discharge for Rectangular Weir							
Beginning Elevation							
FL Discharge	Elevation	Increment	Top of Basin				
345.50	345.50	1.00	353.50				

Stage	Head (H)	Weir Length (L)	Area (A)	Orifice Coefficient (C)	Velocity	Discharge (Q
Jiage	ricau (ii)	(L)	Alea (A)	(0)	velocity	Discharge (G
msl	ft	ft	sf		ft/s	cfs
345.50	0.00	0.42	0.00	3.33	0.00	0.00
346.50	1.00	0.42	0.42	3.33	3.33	1.40
347.50	2.00	0.42	0.84	3.33	4.71	3.96
348.50	3.00	0.42	1.26	3.33	5.77	7.27
349.50	4.00	0.42	1.68	3.33	6.66	11.19
350.50	5.00	0.42	2.10	3.33	7.45	15.64
351.50	6.00	0.42	2.52	3.33	8.16	20.56
352.50	7.00	0.42	2.94	3.33	8.81	25.90
353.50	8.00	0.42	3.36	3.33	9.42	31.65

#### **Storage Indication Curve**



### **Alternate Routing Time**

The following spreadsheets represent the Hydrograph Routing for the various storm events. In each case, the Routing Storm Duration time was adjusted to provide the maximum storage required. Also, runoff coefficients C have been adjusted for each storm event:

Storm Event	Pre C	Post C	
2	0.41	0.47	
5	0.44	0.50	
10	0.47	0.53	
25	0.52	0.58	
50	0.55	0.61	
100	0.59	0.66	

Coefficients for Storage Indication Curve from Chart							
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx				
0.0001	-0.0049	0.2657	5.6215				

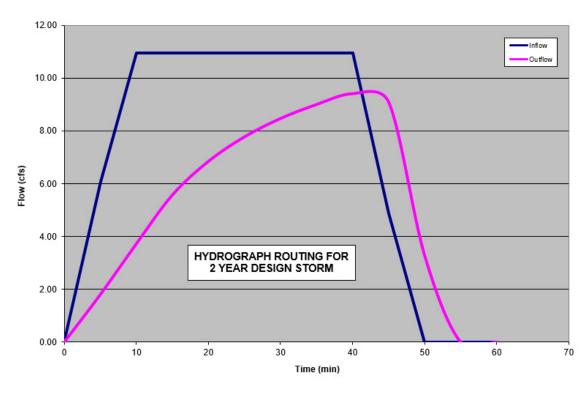
#### HYDROGRAPH ROUTING FOR 2 YEAR DESIGN STORM

**Routing Storm Duration** 

20	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	15.97	0	15.973	0	0	15.972	0.001
5	8.87	24.85	10.876	35.723	2.548	2013.7	35.724	-0.001
10	15.97	31.95	25.334	57.280	5.194	4579.3	57.280	0.000
15	15.97	31.95	41.818	73.764	7.731	7432.4	73.764	-0.001
20	15.97	23.07	54.737	77.809	9.513	9637.5	77.810	-0.001
25	7.10	7.10	57.939	65.038	9.935	10181.1	8.503	56.535
30	0.00	0.00	62.199	62.199	1.520	9527.8	0.000	62.199
35	0.00	0.00	50.999	50.999	0.000	9329.8	0.000	50.999
40	0.00	0.00	51.199	51.199	0.000	7649.8	0.000	51.199
45	0.00	0.00	51.399	51.399	0.000	7679.8	0.000	51.399
50	0.00	0.00	51.599	51.599	0.000	7709.8	0.000	51.599
55	0.00	0.00	51.799	51.799	0.000	7739.8	0.000	51.799
60	0.00	0.00	51.999	51.999	0.000	7769.8	0.000	51.999

Actual Maximum Storage needed is 10181.1 cubic feet
Maximum Storage required is achieved at an elev. = 349.32
Maximum Allowable (undeveloped) Discharge is 11.99 cfs
Maximum Discharge for the above storm is 9.93 cfs

#### **DETENTION HYDROGRAPH**



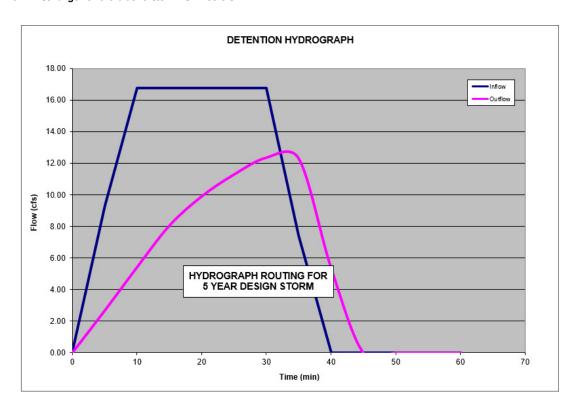
ſ	Coefficients for Storage Indication Curve from Chart							
	$Ax^4$	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx				
ı	0.0001	-0.0049	0.2657	5.6215				

#### **HYDROGRAPH ROUTING FOR 5 YEAR DESIGN STORM**

**Routing Storm Duration** 

30	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	16.75	0	16.750	0	0	16.749	0.001
5	9.31	26.06	11.428	37.484	2.661	2113.4	37.485	-0.001
10	16.75	33.50	26.658	60.157	5.413	4810.6	60.158	-0.001
15	16.75	33.50	44.056	77.555	8.051	7816.0	77.555	0.001
20	16.75	33.50	57.739	91.238	9.908	10147.0	91.236	0.002
25	16.75	33.50	68.648	102.147	11.295	11991.4	102.146	0.001
30	16.75	24.19	77.420	101.614	12.364	13467.5	101.615	-0.001
35	7.44	7.44	76.989	84.434	12.312	13395.2	36.484	47.950
40	0.00	0.00	73.856	73.856	5.389	11856.7	0.000	73.856
45	0.00	0.00	74.056	74.056	0.000	11078.4	0.000	74.056
50	0.00	0.00	74.256	74.256	0.000	11108.4	0.000	74.256
55	0.00	0.00	74.456	74.456	0.000	11138.4	0.000	74.456
60	0.00	0.00	74.656	74.656	0.000	11168.4	0.000	74.656

Actual Maximum Storage needed is 13467.5 cubic feet
Maximum Storage required is achieved at an elev. = 349.89
Maximum Allowable (undeveloped) Discharge is 14.9 cfs
Maximum Discharge for the above storm is 12.36 cfs



Coefficients for Storage Indication Curve from Chart							
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx				
0.0001	-0.0049	0.2657	5.6215				

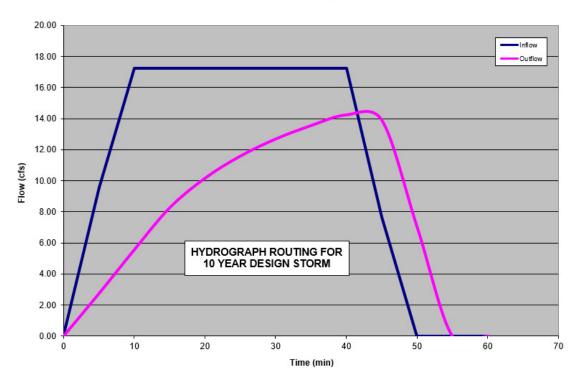
#### HYDROGRAPH ROUTING FOR 10 YEAR DESIGN STORM

**Routing Storm Duration** 

40	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	17.24	0	17.240	0	0	17.239	0.001
5	9.58	26.82	11.778	38.596	2.731	2176.3	38.597	-0.001
10	17.24	34.48	27.496	61.977	5.550	4956.9	61.976	0.001
15	17.24	34.48	45.475	79.956	8.251	8058.9	79.956	0.000
20	17.24	34.48	59.644	94.124	10.156	10469.9	94.123	0.001
25	17.24	34.48	70.962	105.442	11.581	12381.4	105.442	0.000
30	17.24	34.48	80.081	114.561	12.681	13914.2	114.560	0.001
35	17.24	34.48	87.472	121.953	13.544	15152.5	121.953	0.000
40	17.24	24.90	93.489	118.391	14.232	16158.1	118.390	0.001
45	7.66	7.66	90.587	98.249	13.902	15673.3	50.238	48.011
50	0.00	0.00	84.384	84.384	7.032	13682.5	0.000	84.384
55	0.00	0.00	84.584	84.584	0.000	12657.6	0.000	84.584
60	0.00	0.00	84.784	84.784	0.000	12687.6	0.000	84.784

Actual Maximum Storage needed is 16158.1 cubic feet
Maximum Storage required is achieved at an elev. = 350.25
Maximum Allowable (undeveloped) Discharge is 17.36 cfs
Maximum Discharge for the above storm is 14.23 cfs

#### **DETENTION HYDROGRAPH**



Coefficients for Storage Indication Curve from Chart							
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx				
0.0001	-0.0049	0.2657	5.6215				

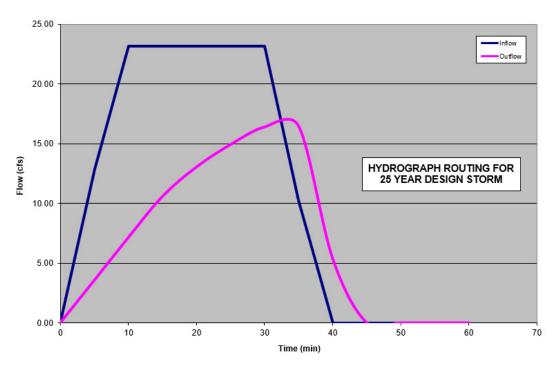
#### **HYDROGRAPH ROUTING FOR 25 YEAR DESIGN STORM**

**Routing Storm Duration** 

30	minutes							
	 1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	23.16	0	23.158	0	0	23.159	-0.001
5	12.87	36.02	16.041	52.065	3.559	2939.9	52.066	-0.001
10	23.16	46.32	37.780	84.097	7.142	6738.4	84.098	-0.001
15	23.16	46.32	62.939	109.256	10.579	11027.7	109.256	0.000
20	23.16	46.32	83.168	129.485	13.044	14431.8	129.484	0.001
25	23.16	46.32	99.641	145.958	14.922	17184.4	145.957	0.001
30	23.16	33.45	113.166	146.617	16.396	19434.3	146.616	0.001
35	10.29	10.29	113.708	124.001	16.454	19524.4	36.239	87.762
40	0.00	0.00	113.484	113.484	5.359	17796.3	0.000	113.484
45	0.00	0.00	113.684	113.684	0.000	17022.6	0.000	113.684
50	0.00	0.00	113.884	113.884	0.000	17052.6	0.000	113.884
55	0.00	0.00	114.084	114.084	0.000	17082.6	0.000	114.084
60	0.00	0.00	114.284	114.284	0.000	17112.6	0.000	114.284

Actual Maximum Storage needed is 19524.4 cubic feet
Maximum Storage required is achieved at an elev. = 350.65
Maximum Allowable (undeveloped) Discharge is 19.53 cfs
Maximum Discharge for the above storm is 16.45 cfs

#### DETENTION HYDROGRAPH



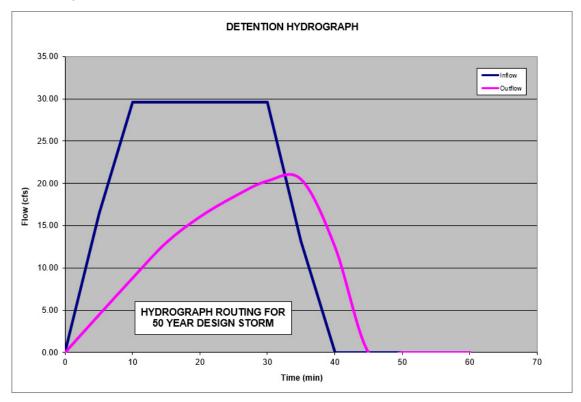
Coefficients	for Storage In	dication Curve	from Chart
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
0.0001	-0.0049	0.2657	5.6215

#### **HYDROGRAPH ROUTING FOR 50 YEAR DESIGN STORM**

**Routing Storm Duration** 

30	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	29.62	0	29.616	0	0	29.615	0.001
5	16.45	46.07	20.781	66.850	4.417	3779.8	66.850	0.000
10	29.62	59.23	49.291	108.522	8.779	8710.6	108.523	-0.001
15	29.62	59.23	82.573	141.804	12.974	14332.1	141.804	0.000
20	29.62	59.23	109.747	168.978	16.029	18866.3	168.978	0.000
25	29.62	59.23	132.202	191.433	18.388	22588.5	191.434	0.000
30	29.62	42.78	150.904	193.682	20.265	25675.3	193.683	-0.001
35	13.16	13.16	152.783	165.945	20.449	25984.8	102.860	63.085
40	0.00	0.00	141.080	141.080	12.532	23011.9	0.000	141.080
45	0.00	0.00	141.280	141.280	0.000	21162.0	0.000	141.280
50	0.00	0.00	141.480	141.480	0.000	21192.0	0.000	141.480
55	0.00	0.00	141.680	141.680	0.000	21222.0	0.000	141.680
60	0.00	0.00	141.880	141.880	0.000	21252.0	0.000	141.880

Actual Maximum Storage needed is 25984.8 cubic feet
Maximum Storage required is achieved at an elev. = 351.37
Maximum Allowable (undeveloped) Discharge is 25.68 cfs
Maximum Discharge for the above storm is 20.45 cfs



Coefficients	for Storage In	dication Curve	from Chart
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
0.0001	-0.0049	0.2657	5.6215

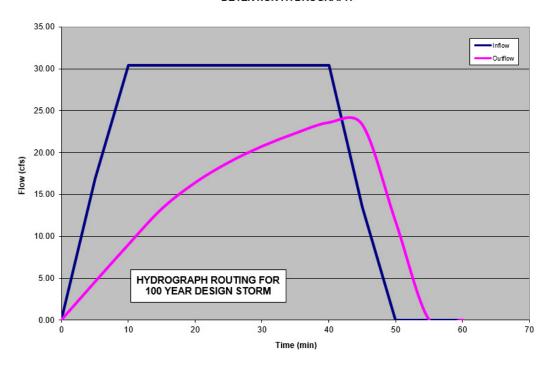
#### HYDROGRAPH ROUTING FOR 100 YEAR DESIGN STORM

**Routing Storm Duration** 

40	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	30.44	0	30.441	0	0	30.440	0.001
5	16.91	47.35	21.393	68.745	4.524	3887.5	68.746	-0.001
10	30.44	60.88	50.780	111.662	8.983	8964.4	111.661	0.001
15	30.44	60.88	85.119	146.000	13.272	14758.5	146.001	-0.001
20	30.44	60.88	113.200	174.082	16.400	19440.0	174.083	-0.001
25	30.44	60.88	136.442	197.324	18.820	23289.3	197.323	0.001
30	30.44	60.88	155.829	216.711	20.747	26486.5	216.710	0.001
35	30.44	60.88	172.091	232.972	22.310	29160.1	232.973	-0.001
40	30.44	43.97	185.788	229.759	23.592	31407.1	229.758	0.001
45	13.53	13.53	183.077	196.607	23.341	30962.7	94.375	102.232
50	0.00	0.00	173.395	173.395	11.706	27735.1	0.000	173.395
55	0.00	0.00	173.595	173.595	0.000	26009.2	0.000	173.595
60	0.00	0.00	173.795	173.795	0.000	26039.2	0.000	173.795

Actual Maximum Storage needed is 31407.1 cubic feet
Maximum Storage required is achieved at an elev. = 352.03
Maximum Allowable (undeveloped) Discharge is 29.36 cfs
Maximum Discharge for the above storm is 23.59 cfs

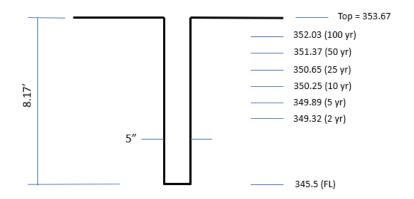
#### DETENTION HYDROGRAPH



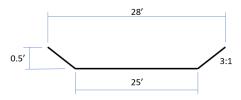
# **Summary – Detention**

Storm Event	Volume Needed (cf)	WSE	Max Discharge Allowed (cfs)	Max Discharge Model (cfs)
2	10181.1	349.32	11.99	9.93
5	13467.5	349.89	14.90	12.36
10	16158.1	350.25	17.36	14.23
25	19524.4	350.65	19.53	16.45
50	25984.8	351.37	25.68	20.45
100	31407.1	352.03	29.36	23.59

# **Discharge Structure Detail**



#### **Overflow Structure Detail**



 $Q = (1.49/n)(A)(R^2/3)(S^0.5)$ 

Q = (1.49/0.025)(13.25)(0.60)(0.1) = 47.38 cfs

Required Capacity = 23.59 cfs (2) = 47.18 cfs

# **Study Point Summary (25 yr Storm)**



Study Point	Pre Construction	<b>Post Construction</b>	Post Construction	Change - Pre to Post
	Q	Q (no detention)	Q (with detention)	(with detention)
	(cfs)	(cfs)	(cfs)	(cfs)
Α	12.88	16.81	16.81	3.93
В	10.53	0	0	-10.53
С	11.01	0	0	-11.01
<u>D</u>	<u>17.74</u>	<u>38.08</u>	<u>16.45</u>	<u>-1.29</u>
TOTAL	52.16	54.89	33.26	-18.9

<sup>\*</sup> Existing culvert originating at the Junction Box near the NE corner of Hurricane Gardens has adequate capacity to accept this slight increase in flow.

# **Downstream Considerations**

The discharge from the proposed Detention Facility will enter into an existing ditch that drains to the West, into Hurricane Lake, Phase 3. The ditch exists between Lots 47 and 48 of said development (based on Saline County GIS map). A 54" CMP (Helical) culvert exists under Worth Ave, at a grade of 0.7% (as shot in the field). Using an n of 0.012, the capacity of this culvert is computed at 183.65 cfs at d/D of 0.85 (velocity = 12.75 fps). It should be noted that the estimated post construction discharge is 1.29 cfs less than the estimated existing runoff from the same area. Therefore, this development should not have a negative impact on the downstream properties.



Source: Saline County GIS

# **Engineering Certification**

I, Tim Lemons, Arkansas Registered Professional Engineer No. 7373, hereby certify that the drainage reports, and calculations contained in this report, have been prepared in accordance with sound engineering practice and principles, and based on best known available data. Improvements as outlined in this report and depicted on the preliminary plat and design drawings should not increase the risk of endangerment to life or have negative impacts on adjacent or downstream property or watersheds.



Timothy B. Lemons, PE Arkansas Professional Engineer, #7373

# **Appendix**

Clara -	. O E0/ -	- 0 013						
siope =	= 0.5%, r	n = 0.012						
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)	·	(ft)	(sf)					(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.00500	0.0707	0.00
1	0.030	0.03	0.02	0.01	0.06	0.00500	0.0707	0.01
1.5	0.030	0.05	0.03	0.02	0.08	0.00500	0.0707	0.02
2	0.030	0.06	0.06	0.03	0.10	0.00500	0.0707	0.05
2.5	0.030	0.08	0.09	0.04	0.11	0.00500	0.0707	0.09
3	0.030	0.09	0.14	0.04	0.13	0.00500	0.0707	0.15
3.5	0.030	0.11	0.18	0.05	0.14	0.00500	0.0707	0.22
4	0.030	0.12	0.24	0.06	0.15	0.00500	0.0707	0.32
4.5	0.030	0.14	0.30	0.07	0.16	0.00500	0.0707	0.44
5	0.030	0.15	0.38	0.07	0.18	0.00500	0.0707	0.58
5.5	0.030	0.17	0.45	0.08	0.19	0.00500	0.0707	0.75
6	0.030	0.18	0.54	0.09	0.20	0.00500	0.0707	0.94
6.5	0.030	0.20	0.63	0.10	0.21	0.00500	0.0707	1.17
7	0.030	0.21	0.74	0.10	0.22	0.00500	0.0707	1.43
7.5	0.030	0.23	0.84	0.11	0.23	0.00500	0.0707	1.71
8.5	0.030	0.26	1.08	0.13	0.25	0.00500	0.0707	2.39
9	0.030	0.27	1.22	0.13	0.26	0.00500	0.0707	2.79
9.5	0.030	0.29	1.35	0.14	0.27	0.00500	0.0707	3.22
10	0.030	0.30	1.50	0.15	0.28	0.00500	0.0707	3.69
10.5	0.030	0.32	1.65	0.16	0.29	0.00500	0.0707	4.21
11	0.030	0.33	1.82	0.16	0.30	0.00500	0.0707	4.76
11.5	0.030	0.35	1.98	0.17	0.31	0.00500	0.0707	5.36
12	0.030	0.36	2.16	0.18	0.32	0.00500	0.0707	6.01
12.5	0.030	0.38	2.34	0.19	0.33	0.00500	0.0707	6.70
13	0.030	0.39	2.54	0.19	0.33	0.00500	0.0707	7.44

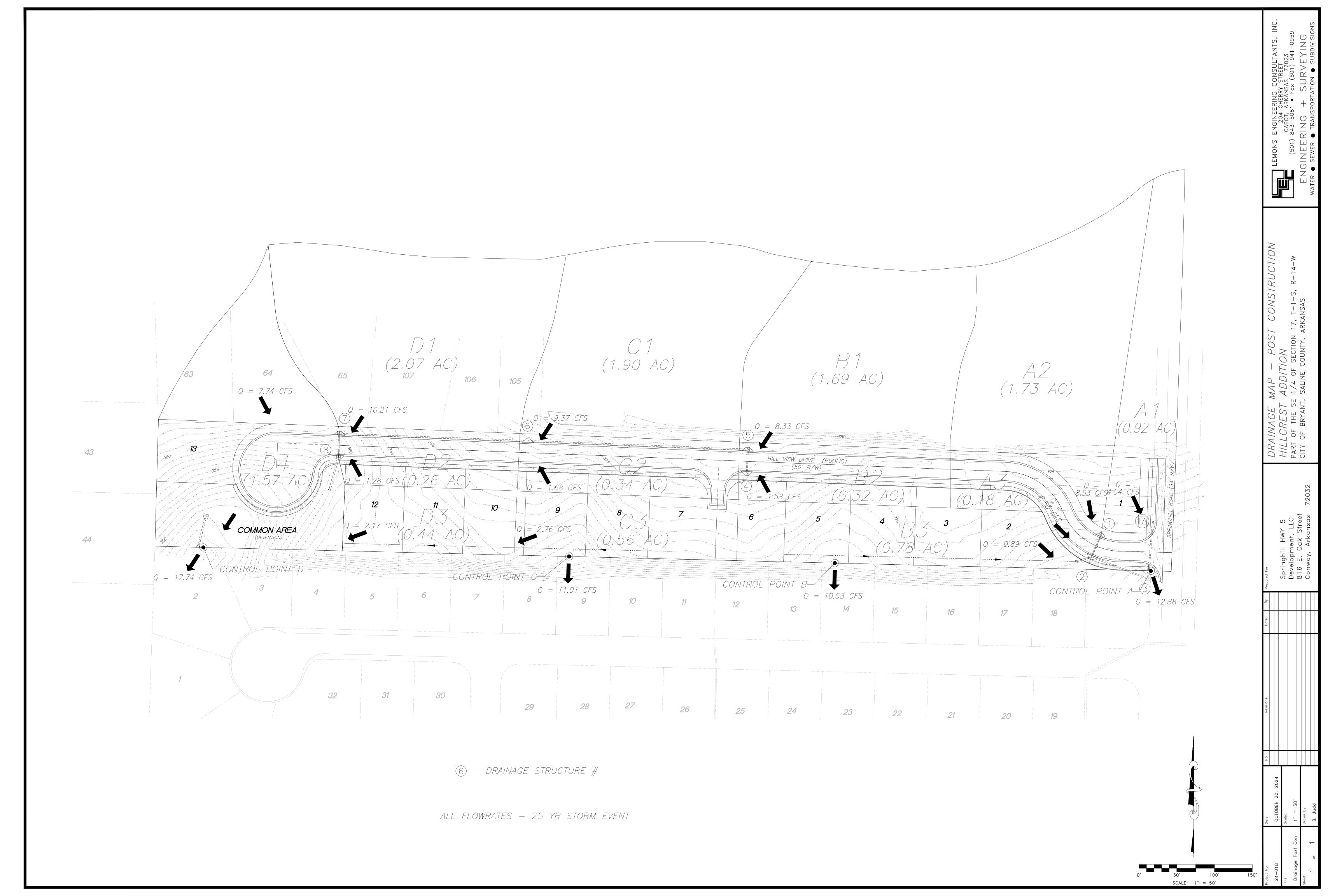
Slope =	= 1.50%	n = 0.012	2					
J. 0 P C	,	. 0.02.	_					
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)		(ft)	(sf)					(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.01500	0.1225	0.00
1	0.030	0.03	0.02	0.01	0.06	0.01500	0.1225	0.01
1.5	0.030	0.05	0.03	0.02	0.08	0.01500	0.1225	0.04
2	0.030	0.06	0.06	0.03	0.10	0.01500	0.1225	0.09
2.5	0.030	0.08	0.09	0.04	0.11	0.01500	0.1225	0.16
3	0.030	0.09	0.14	0.04	0.13	0.01500	0.1225	0.26
3.5	0.030	0.11	0.18	0.05	0.14	0.01500	0.1225	0.39
4	0.030	0.12	0.24	0.06	0.15	0.01500	0.1225	0.55
4.5	0.030	0.14	0.30	0.07	0.16	0.01500	0.1225	0.76
5	0.030	0.15	0.38	0.07	0.18	0.01500	0.1225	1.01
5.5	0.030	0.17	0.45	0.08	0.19	0.01500	0.1225	1.30
6	0.030	0.18	0.54	0.09	0.20	0.01500	0.1225	1.64
6.5	0.030	0.20	0.63	0.10	0.21	0.01500	0.1225	2.03
7	0.030	0.21	0.74	0.10	0.22	0.01500	0.1225	2.47
7.5	0.030	0.23	0.84	0.11	0.23	0.01500	0.1225	2.97
8.5	0.030	0.26	1.08	0.13	0.25	0.01500	0.1225	4.15
9	0.030	0.27	1.22	0.13	0.26	0.01500	0.1225	4.83
9.5	0.030	0.29	1.35	0.14	0.27	0.01500	0.1225	5.58
10	0.030	0.30	1.50	0.15	0.28	0.01500	0.1225	6.40
10.5	0.030	0.32	1.65	0.16	0.29	0.01500	0.1225	7.29
11	0.030	0.33	1.82	0.16	0.30	0.01500	0.1225	8.25
11.5	0.030	0.35	1.98	0.17	0.31	0.01500	0.1225	9.29
12	0.030	0.36	2.16	0.18	0.32	0.01500	0.1225	10.41
12.5	0.030	0.38	2.34	0.19	0.33	0.01500	0.1225	11.61
13	0.030	0.39	2.54	0.19	0.33	0.01500	0.1225	12.89

		ITY OF ST		Z/ BCT	U DC			
Slope =	2.67%,	n = 0.012	2					
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)	Siope	(ft)	(sf)	I N	K-2/3	3	3-1/2	(cfs)
(10)		(10)	(31)					(613)
0.5	0.030	0.02	0.00	0.01	0.04	0.02670	0.1634	0.00
1	0.030	0.03	0.02	0.01	0.06	0.02670	0.1634	0.02
1.5	0.030	0.05	0.03	0.02	0.08	0.02670	0.1634	0.05
2	0.030	0.06	0.06	0.03	0.10	0.02670	0.1634	0.12
2.5	0.030	0.08	0.09	0.04	0.11	0.02670	0.1634	0.21
3	0.030	0.09	0.14	0.04	0.13	0.02670	0.1634	0.34
3.5	0.030	0.11	0.18	0.05	0.14	0.02670	0.1634	0.52
4	0.030	0.12	0.24	0.06	0.15	0.02670	0.1634	0.74
4.5	0.030	0.14	0.30	0.07	0.16	0.02670	0.1634	1.01
5	0.030	0.15	0.38	0.07	0.18	0.02670	0.1634	1.34
5.5	0.030	0.17	0.45	0.08	0.19	0.02670	0.1634	1.73
6	0.030	0.18	0.54	0.09	0.20	0.02670	0.1634	2.18
6.5	0.030	0.20	0.63	0.10	0.21	0.02670	0.1634	2.70
7	0.030	0.21	0.74	0.10	0.22	0.02670	0.1634	3.29
7.5	0.030	0.23	0.84	0.11	0.23	0.02670	0.1634	3.96
8.5	0.030	0.26	1.08	0.13	0.25	0.02670	0.1634	5.53
9	0.030	0.27	1.22	0.13	0.26	0.02670	0.1634	6.44
9.5	0.030	0.29	1.35	0.14	0.27	0.02670	0.1634	7.44
10	0.030	0.30	1.50	0.15	0.28	0.02670	0.1634	8.53
10.5	0.030	0.32	1.65	0.16	0.29	0.02670	0.1634	9.72
11	0.030	0.33	1.82	0.16	0.30	0.02670	0.1634	11.01
11.5	0.030	0.35	1.98	0.17	0.31	0.02670	0.1634	12.40
12	0.030	0.36	2.16	0.18	0.32	0.02670	0.1634	13.89
12.5	0.030	0.38	2.34	0.19	0.33	0.02670	0.1634	15.49
13	0.030	0.39	2.54	0.19	0.33	0.02670	0.1634	17.20

		ITY OF ST						
oope =	4.88%,	n = 0.012						
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)		(ft)	(sf)		•			(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.04880	0.2209	0.00
1	0.030	0.03	0.02	0.01	0.06	0.04880	0.2209	0.02
1.5	0.030	0.05	0.03	0.02	0.08	0.04880	0.2209	0.07
2	0.030	0.06	0.06	0.03	0.10	0.04880	0.2209	0.16
2.5	0.030	0.08	0.09	0.04	0.11	0.04880	0.2209	0.28
3	0.030	0.09	0.14	0.04	0.13	0.04880	0.2209	0.46
3.5	0.030	0.11	0.18	0.05	0.14	0.04880	0.2209	0.70
4	0.030	0.12	0.24	0.06	0.15	0.04880	0.2209	1.00
4.5	0.030	0.14	0.30	0.07	0.16	0.04880	0.2209	1.37
5	0.030	0.15	0.38	0.07	0.18	0.04880	0.2209	1.81
5.5	0.030	0.17	0.45	0.08	0.19	0.04880	0.2209	2.34
6	0.030	0.18	0.54	0.09	0.20	0.04880	0.2209	2.95
6.5	0.030	0.20	0.63	0.10	0.21	0.04880	0.2209	3.65
7	0.030	0.21	0.74	0.10	0.22	0.04880	0.2209	4.45
7.5	0.030	0.23	0.84	0.11	0.23	0.04880	0.2209	5.35
8.5	0.030	0.26	1.08	0.13	0.25	0.04880	0.2209	7.48
9	0.030	0.27	1.22	0.13	0.26	0.04880	0.2209	8.71
9.5	0.030	0.29	1.35	0.14	0.27	0.04880	0.2209	10.06
10	0.030	0.30	1.50	0.15	0.28	0.04880	0.2209	11.54
10.5	0.030	0.32	1.65	0.16	0.29	0.04880	0.2209	13.14
11	0.030	0.33	1.82	0.16	0.30	0.04880	0.2209	14.88
11.5	0.030	0.35	1.98	0.17	0.31	0.04880	0.2209	16.76
12	0.030	0.36	2.16	0.18	0.32	0.04880	0.2209	18.77
12.5	0.030	0.38	2.34	0.19	0.33	0.04880	0.2209	20.94
13	0.030	0.39	2.54	0.19	0.33	0.04880	0.2209	23.25



ALL FLOWRATES — 25 YR STORM EVENT



# **Drainage Report**

For

# **Hillcrest Addition**

Springhill Road Bryant, Arkansas

Revised: October 21, 2024

# Prepared By:



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# **Project Information**

Project Title: Hillcrest Addition

**Project Description:** 13 lot single family development located on the West side of

Springhill Road, North of and adjacent to Hurricane Gardens,

Bryant, Arkansas (address: 3927 Springhill Road)

Owner/Developer: Springhill – Hwy 5 Development, LLC

816 East Oak Street

Conway, Arkansas 72032

**Engineer of Record:** Lemons Engineering Consultants, Inc.

Tim Lemons, PE 204 Cherry Street

Cabot, Arkansas 72023

(501) 605-7565

# **General Information**

This proposed development shall include 13 single family lots. This property is essentially the Northern Most tract of land within the city limits of Bryant as it presently exist. The property to the North of the subject site is developed with duplex style residential structures existing outside the City limits of Bryant. The property to the South is an established subdivision (Hurricane Gardens). The property drains North to South. There have been several reports of drainage issues by the residents of Hurricane Gardens. At present, the drainage from the subject property, and that to the north of the subject property, flows onto Hurricane Gardens. No detention exists on the property located north of the subject property.

#### The objectives of this report are as follows:

- Determine the estimated increase in runoff due to the development of Hillcrest Addition.
- 2) Provide design computations for a detention facility to bring the runoff from said tract to pre-construction rate.
- 3) Based on comments expressed by the residents, divert as much flow as possible away from the rear of the Northern most lots within Hurricane Gardens. As previously stated, the majority of the property to the North of Hurricane Gardens flows into the rear of the Northern most lots, creating an issue for the property owners.
- 4) Size the infrastructure in the development using the City's Drainage Code.
- 5) Compare the estimated Pre and Post flowrates at specific control points to show that the overall runoff from Hillcrest is at or less than the pre-construction flowrate.

The control points (A-D) to be used in this analysis are shown on the following vicinity map, and throughout this report.

# **Project Vicinity Map**



# **Hydrological Computations**

For this analysis, we will use the Rational Method in determining culvert sizes, culvert capacity computations, and other related issues on site. The total watershed size for this development is estimated at 12.40 acres. Attention is called to the Watershed Map included in this report. As per the Rational Method, the following equation is used:

Q = C x I x A, where:

Q = Flowrate (cfs)

C = Runoff Coefficient

I = Intensity (from tables)

A = area (acres)

The selection of the appropriate intensity is based on the estimated time of concentration (tc).

#### **Determination of Runoff Coefficients "C"**

In determining the Pre Construction C, we must consider the property to the North that is developed, and discharging onto the subject property. The C factor for Pre and Post Conditions are based on Table 400-1 "Runoff Coefficients for Surface Types" as provided in the Bryant Drainage Manual. A factored (weighted) value of C is determined in the following tables:

#### **Pre Construction Conditions**

Storm Event	Off Site C1	Off Site A1 (acres)	Off Site C2	Off Site A2 (acres)	On Site C3	On Site A3 (acres)	On Site C4	On Site A4 (acres)	Weighted C Factor
2	0.75	3.04	0.29	4.73	0.75	0.19	0.29	4.59	0.41
5	0.8	3.04	0.32	4.73	0.8	0.19	0.32	4.59	0.44
10	0.83	3.04	0.35	4.73	0.83	0.19	0.35	4.59	0.47
25	0.88	3.04	0.39	4.73	0.88	0.19	0.39	4.59	0.52
50	0.92	3.04	0.42	4.73	0.92	0.19	0.42	4.59	0.55
100	0.97	3.04	0.46	4.73	0.97	0.19	0.46	4.59	0.59

C1 (off site for homes, streets, etc.)

C2 (off site for grass, landscaping, etc.)

C3 (on site for homes, streets, etc.)

C4 (on site for grass. Landscaping, etc.)

A1 (off site area for C1)

A2 (off site area for C2)

A3 (on site area for C3)

A4 (on site area for C4)

#### **Post Construction Conditions**

Storm Event	Off Site	Off Site	Off Site	Off Site	On Site	On Site	On Site	On Site	Weighted
	C1	A1	C2	A2	C3	А3	C4	A4	С
		(acres)		(acres)		(acres)		(acres)	Factor
2	0.75	3.04	0.29	4.73	0.75	1.81	0.29	3.07	0.47
5	8.0	3.04	0.32	4.73	0.8	1.81	0.32	3.07	0.50
10	0.83	3.04	0.35	4.73	0.83	1.81	0.35	3.07	0.53
25	0.88	3.04	0.39	4.73	0.88	1.81	0.39	3.07	0.58
50	0.92	3.04	0.42	4.73	0.92	1.81	0.42	3.07	0.61
100	0.97	3.04	0.46	4.73	0.97	1.81	0.46	3.07	0.66

C1 (off site for homes, streets, etc.)

C2 (off site for grass, landscaping, etc.)

C3 (on site for homes, streets, etc.)

C4 (on site for grass. Landscaping, etc.)

A1 (off site area for C1)

A2 (off site area for C2)

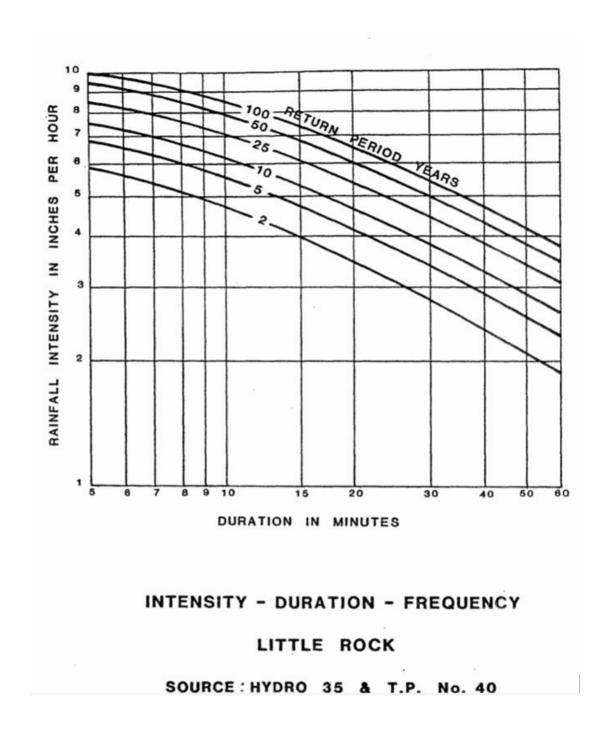
A3 (on site area for C3)

A4 (on site area for C4)

The above variable values will be used in designing the Detention Facility. For culvert design, we will use the Post C values for the 25 year storm.

# **Determination of Intensity Values "I"**

For this analysis, we will use the Intensity – Duration - Frequency Chart from the Little Rock Drainage Manual. Whereas the calculated value of I shall be used for Detention, we will use a tc (time of concentration) of 5 min for the culverts to also provide a conservative value.



# **Drainage Map (Pre-Construction)**



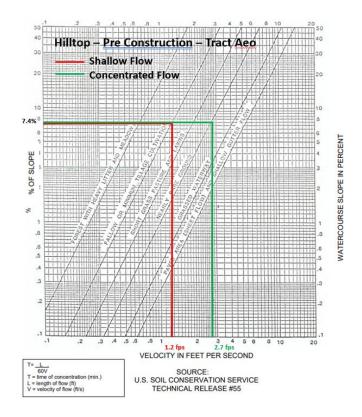
See attached map for additional information

# **Pre Construction Flowrates – Control Points**

The estimated Pre Construction Flowrate for each Control Point is estimated as follows. These values will be used to compare to the Post Construction Flowrate later in this report:

#### **Control Point A**

The time of concentration is determined as follows:



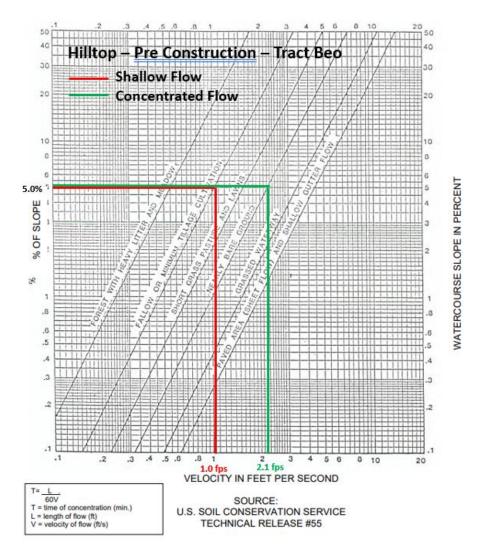
$$tc = ((300)/(60)(1.2)) + ((300)/(60)(2.7)) = 6 min$$

Flowrates for various Storm Events (Control Point A):

Storm Event	С	tc	ı	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	6	5.6	3.02	6.93
5	0.44	6	6.6	3.02	8.77
10	0.47	6	7.3	3.02	10.36
25	0.52	6	8.2	3.02	12.88
50	0.55	6	9.2	3.02	15.28
100	0.59	6	9.8	3.02	17.46

#### **Control Point B**

The time of concentration is determined as follows:



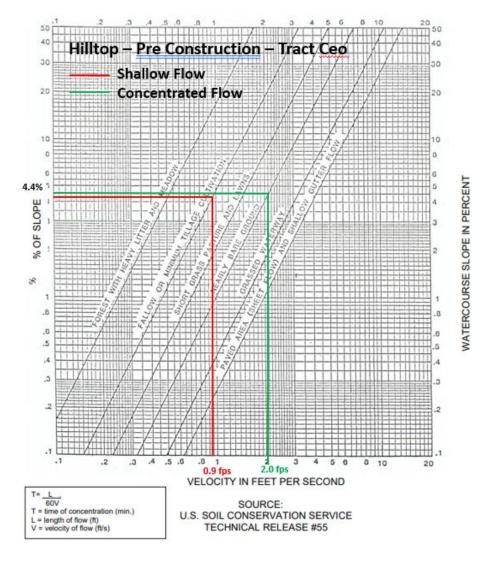
$$tc = ((300)/(60)(1.0)) + ((200)/(60)(2.1)) = 6.5 min$$

Flowrates for various Storm Events (Control Point B):

Storm Event	С	tc	Į.	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	6.5	5.6	2.47	5.67
5	0.44	6.5	6.6	2.47	7.17
10	0.47	6.5	7.3	2.47	8.47
25	0.52	6.5	8.2	2.47	10.53
50	0.55	6.5	9.2	2.47	12.50
100	0.59	6.5	9.8	2.47	14.28

#### **Control Point C**

The time of concentration is determined as follows:



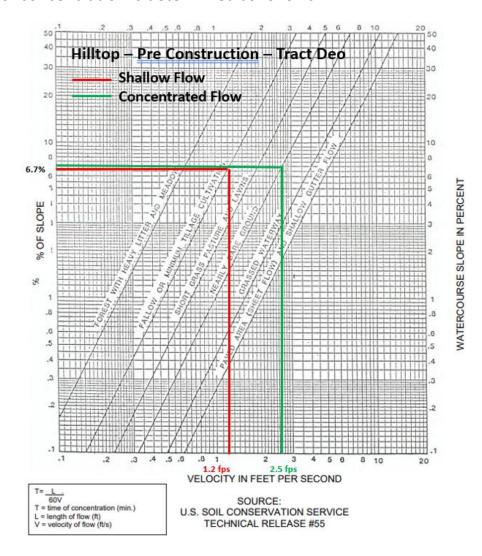
$$tc = ((300)/(60)(0.9)) + ((300)/(60)(2.0)) = 8 min$$

#### Flowrates for various Storm Events (Control Point C):

Storm Event	С	tc	I	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	8	5.1	2.75	5.75
5	0.44	8	6	2.75	7.26
10	0.47	8	6.7	2.75	8.66
25	0.52	8	7.7	2.75	11.01
50	0.55	8	8.5	2.75	12.86
100	0.59	8	9.1	2.75	14.76

#### **Control Point D**

The time of concentration is determined as follows:



$$tc = ((300)/(60)(1.2)) + ((340)/(60)(2.5)) = 6.4 min$$

Flowrates for various Storm Events (Control Point D):

Storm Event	С	tc	I	Α	Q
		(min)	(in/hour)	(acres)	(cfs)
2	0.41	6.5	5.6	4.16	9.55
5	0.44	6.5	6.6	4.16	12.08
10	0.47	6.5	7.3	4.16	14.27
25	0.52	6.5	8.2	4.16	17.74
50	0.55	6.5	9.2	4.16	21.05
100	0.59	6.5	9.8	4.16	24.05

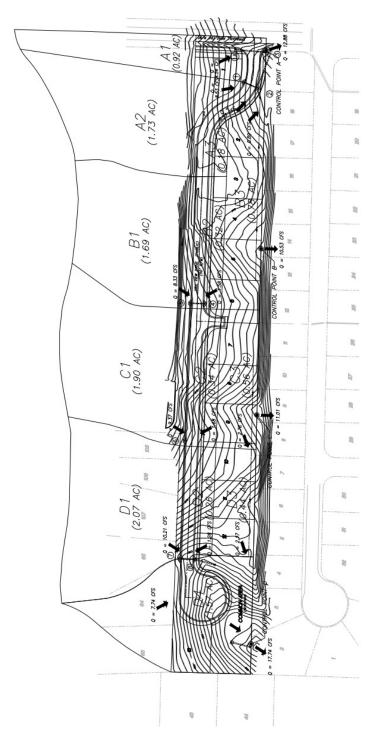
# **Determination of Flowrates for Culverts & Spreadflow**

Attention is called to the following chart which provides C, Intensity, Area, and Flowrate (Q) of each Tract. Again, the Rational Method is being used for all basins. Attention is called to the Maps on the next two pages for a detailed drawings showing the various watershed tracts. The 25 year storm event will be used for culvert design. A conservative tc of 5 minutes is used for the culvert design.

Tract	C(Post)	125	Α	Q25
		(in/hr)	(ac)	(cfs)
A1	0.58	8.5	0.92	4.54
A2	0.58	8.5	1.73	8.53
A3	0.58	8.5	0.18	0.89
B1	0.58	8.5	1.69	8.33
B2	0.58	8.5	0.32	1.58
В3	0.58	8.5	0.78	3.85
C1	0.58	8.5	1.90	9.37
C2	0.58	8.5	0.34	1.68
C3	0.58	8.5	0.56	2.76
D1	0.58	8.5	2.07	10.21
D2	0.58	8.5	0.26	1.28
D3	0.58	8.5	0.44	2.17
D4	0.58	8.5	1.57	7.74

# **Drainage Map (Post Construction)**

#### Revised 10/21/2024



See attached Map for additional information

# **Culvert Sizing**

All culverts are sized to meet a 25 year storm, and the Rational Method is used. We will use a Manning's Coefficient of 0.012 shall be for all culverts (concrete and HDPE). The d/D ratio and velocity was computed using HawsEDC On-Line Calculator (hawsedc.com).

#### FES 1a

Q = Qa1 = 4.54 cfs Use 18" @ 3.5% Q capacity = 21.94 cfs V actual = 9.68 fps (d/D = 0.32)

#### Inlet 1

Q = Qa2 = 8.53 cfs Use 18" @ 1.1% Q capacity = 12.30 cfs V actual = 7.36 fps (d/D = 0.63)

#### Inlet 2

Q = Inlet 1 + Qa3 = 8.53 + 0.89 = 9.42 cfs Use 24" @ 0.3% Q capacity = 13.84 cfs V actual = 4.63 fps (d/D = 0.62)

#### Junction Box 3 (verify capacity)

Q = Inlet 2 + Qb3 + Exist 18" in Hurricane Gardens (Culvert in Hurricane Gardens is an 18" ADS at 0.46%, Capacity = 7.95 cfs at d/D=0.85) Q = 9.42 + 3.85 + 7.95 = 21.22 cfs Existing 24" Discharging from Junc Box is 24" ADS @ 5.20% Q capacity = 57.58 cfs **Capacity appears to exist** V actual = 16.61 fps (d/D = 0.43)

#### Inlet 4

Q = Qb2 = 1.58 cfs Use 18" @ 0.5% Q capacity = 8.29 cfs V actual = 3.53 fps (d/D = 0.30)

#### Inlet 5

Q = Inlet 4 + Qb1 = 1.58 + 8.33 = 9.91 cfs Use 18" @ 1.0% Q capacity = 11.73 cfs V actual = 7.25 fps (d/D = 0.72)

#### Inlet 6

Q = Inlet 5 + Qc1 = 9.91 + 9.37 = 19.28 cfs Use 18" @ 4.60% Q capacity = 25.15 cfs V actual = 15.30 fps (d/D = 0.67)

#### Inlet 7

Q = Inlet 6 + Qd1 = 19.28 + 10.21 = 29.49 cfs Use 24" @ 2.0% Q capacity = 35.71 cfs V actual = 12.38 fps (d/D = 0.71)

#### Inlet 8

Q = Inlet 7 + Qc2 + Qd2 = 29.49 + 1.68 + 1.28 = 32.45 cfs Use 24" @ 2.25% Q capacity = 37.87 cfs V actual = 13.28 fps (d/D = 0.73)

# **Street Spreadflow Analysis & Inlet Capture**

In this Section of the Report, we will examine how the stormwater in the street gutters may impact in proposed inlets. We will use our 27' street width (back of curb to back of curb), while giving allowances for the vertical portion of the curb on each side. The crown on the street shall be 3.0%. The available street width, to handle the stormwater, has a width of 26'. Our goal is to provide a minimum "non submerged" street width ("clear space") of 8 feet. We will use the following equation (as provided in "Urban Drainage and Flood Control District – Urban

Storm Drainage Manual, Volume 1, dated January, 2016) to determine the required length of throat to capture 100% of the stormwater:

```
Lt = 0.38 (Q^0.51)(Sl^0.058)(1/nSx)^0.46, where:
Lt = required length of throat to capture 100%
Q = flowrate (cfs)
Sl = slope of gutter
N = manning's coef. = 0.012
Sx = cross slope of street = 0.03
```

Since n and Sx are constant, the equation can be reduced to:

Lt = 0.38 (Q^0.51)(SI^0.058)(38.38) Lt = 14.58 (Q^0.51) (SI^0.058)

Attention is called to the Appendix for the spreadsheets used to evaluate these areas.

#### Check Inlet 1 & 2 – Hillcrest Drive (Spreadflow Analysis)

#### Inlet 1

Q = Qa2 = 8.53 cfs

Gutter Slope = 1.50%Height of water (from gutter) = 0.33'Width of water (from gutter) = 11.0'Clear space (half street) = 13.0 - 11.0' = 2.0'Inlet 2 Q = Qa3 = 0.89 cfs Gutter Slope = 1.50%Height of water (from gutter) = 0.14'Width of water (from gutter) = 4.5'Clear space (half street) = 13.0 - 4.5' = 8.5'

#### Stormwater Capture - Inlet 1

Total Clear Space = 2.0 + 8.5 = 10.5'

Lt = 14.58 (8.53^0.51)(0.015^0.058) = 34.10 feet Using a 20' throat: Q captured = 5.01 cfs (58.7%) Q bypass = 3.52 cfs (41.3%)

#### **Stormwater Capture – Inlet 2**

Lt = 14.58 (0.89^0.51)(0.015^0.058) = 10.77 feet Using a 12' throat: Q captured = 0.89 cfs (100%) Q bypass = 0.00 cfs (0%)

#### **Check Inlet 4 & 5 – Hillcrest Drive (Spreadflow Analysis)**

#### Inlet 4

Q = Qb2 = 1.58 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.21'

Width of water (from gutter) = 7.0'

Clear space (half street) = 13.0 - 7.0 = 6.0'

#### Inlet 5

Q = Qb1 = 8.33 fps

Gutter Slope = 0.5%

Height of water (from gutter) = 0.39'

Width of water (from gutter) = 13.0'

Clear space (half street) = 13.0 - 13.0' = 0.0'

#### Total Clear Space = 6.0 + 0.0 = 6.0

#### **TRY 10 YEAR STORM**

#### Inlet 4

Q = Qb2 = 1.26 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.20'

Width of water (from gutter) = 6.5'

Clear space (half street) = 13.0 - 6.5' = 6.5'

#### Inlet 5

Q = Qb1 = 6.66 cfs

Gutter Slope = 0.5%

Height of water (from gutter) = 0.36'

Width of water (from gutter) = 12.0'

Clear space (half street) = 13.0 - 12.0' = 1.0'

Total Clear Space = 6.5 + 1.0 = 7.5'

#### Stormwater Capture - Inlet 4

Lt =  $14.58 (1.26^{0.51})(0.005^{0.058}) = 12.06$  feet

Using a 13' throat:

Q captured = 1.26 cfs (100%)

Q bypass = 0.00 cfs (0%)

#### **Stormwater Capture – Inlet 5**

Lt = 14.58 (6.66^0.51)(0.005^0.058) = 28.20 feet

Using a 24' throat:

Q captured = 5.67 cfs (85.1%)

Q bypass = 0.99 cfs (14.9%)

# Check Inlet 6 & Across Street - Hillcrest Drive (Spreadflow Analysis) Inlet 6

Q = Qc1 = 9.37 cfs

Gutter Slope = 2.67%

Height of water (from gutter) = 0.30'

Width of water (from gutter) = 10.0'

Clear space (half street) = 13.0 - 10.0' = 3.0'

#### Across from Inlet 6

Q = Qc2 = 1.68 cfs

Gutter Slope = 2.67%

Height of water (from gutter) = 0.17'

Width of water (from gutter) = 5.5'

Clear space (half street) = 13.0 - 5.5 = 7.5

Total Clear Space = 3.0 + 7.5 = 10.5'

#### Stormwater Capture - Inlet 6

Q = 9.37 + 0.99 (bypass from Inlet 5) = 10.36 cfs

Lt = 14.58 (10.36^0.51)(0.0267^0.058) = 38.93 feet

Using a 30' throat:

Q captured = 7.99 cfs (77.1%)

Q bypass = 2.37 cfs (22.9%)

#### Check Inlet 7 & 8 - Hillcrest (Spreadflow Analysis)

#### Inlet 7

Q = Qd1 = 10.21 cfs

Gutter Slope = 4.88%

Height of water (from gutter) = 0.29'

Width of water (from gutter) = 9.5'

Clear space (half street) = 13.0 - 9.5' = 2.5'

#### Inlet 8

Q = Qc2 + Qd2 = 2.42 + 2.17 = 2.96 cfs

Gutter Slope = 4.88%

Height of water (from gutter) = 0.18'

Width of water (from gutter) = 6.0'

Clear space (half street) = 13.0 - 6.0' = 7.0'

Total Clear Space = 2.5 + 7.0 = 9.5

#### Stormwater Capture – Inlet 7

Q = 10.21 + 2.37 (bypass from Inlet 6) = 12.58 cfs

Lt = 14.58 (12.58^0.51)(0.0488^0.058) = 44.5 feet

Using a 30' throat:

Q captured = 8.48 cfs (67.4%)

Q bypass = 4.10 cfs (0%)

#### **Stormwater Capture – Inlet 8**

Lt = 14.58 (2.96^0.51)(0.0488^0.058) = 21.28 feet Using a 22' throat: Q captured = 21.28 cfs (100%) Q bypass = 0.00 cfs (0%)

#### **Curb Cut on Street at North side of Detention Pond**

Q = Qd4 + 4.10 (bypass from Inlet 7) = 7.74 + 4.10 = 11.84 cfs Use a 6" x 8' Curb Cut with a slope of 3%: Q =  $(1.49/n)(A)(R^2/3)(S^1/2) = (1.49/0.012)(4)(4.33)(0.17) = 22.44$  cfs

# **Detention Facility Computations**

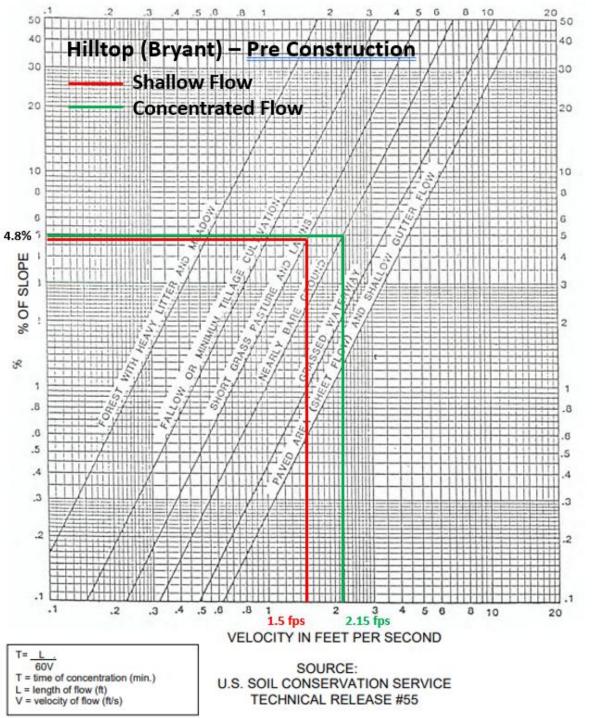
In this section, we will size the detention facility located in the Common Area (West side of the project). At the completion of this section, a summary of pre and post flows will be provided. Whereas the time of concentration will be used to determine the intensity (I), the runoff coefficient (C) for each storm analysis shall be based on that determined on pages 5 and 6 of this report.

# Time of Concentration (tc)

In determining the time of concentration, we must first determine the velocity of the runoff based on the type of ground cover and type of flow. The total tc is a sum of the tc for overland flow, the tc for shallow concentrated flow, and the tc for channelized flow. For this analysis, we will use the US Soil Conservation Service Technical Release #55, "Watercourse Slope vs Velocity" graph. A Pre Construction and Post Construction graph for each watershed is provided on the following pages.

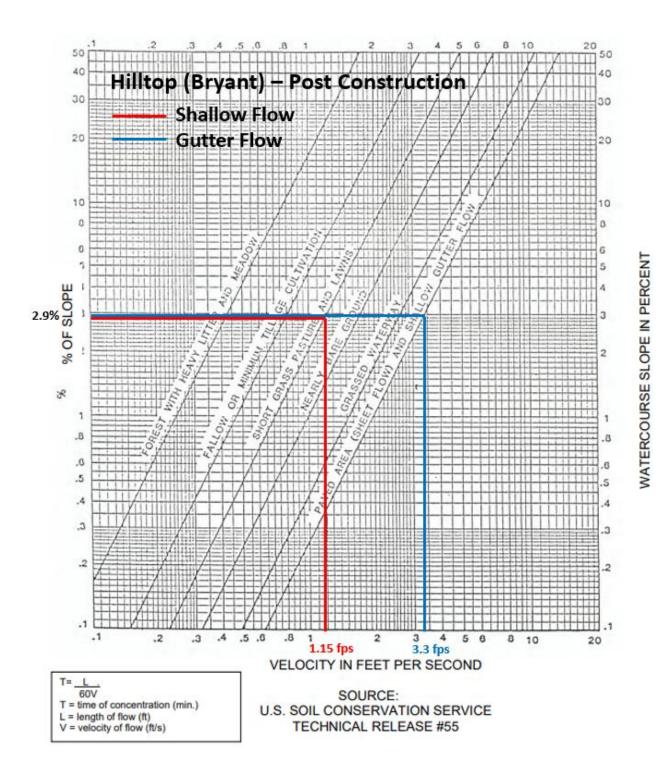
# WATERCOURSE SLOPE IN PERCENT

# **Pre Construction Time of Concentration (tc)**



Pre-Construction tc =  $\Sigma(L/(60)(V))$  = 6 min

# **Post Construction Time of Concentration (tc)**



Post-Construction tc =  $\Sigma(L/(60)(V))$  = 9 min

# **Stage – Storage Table**

The following Stage Storage Table is provided, based on the grading plan contained in the Civil Plans. The accumulative storage is provided in the right most column.

TYPE 3									
Stage - Storage for Irregular Detention Basin									
Top Elev	Bottom Elev	Increment							
353.5	345.5	1							
Stage	Area	Δ Volume	Volume						
msl	sf	cf	cf						
345.50	1	0	0						
346.50	1853.50	927.25	927.25						
347.50	2951.40	2402.45	3329.70						
348.50	4240.13	3595.77	6925.47						
349.50	5637.46	4938.80	11864.26						
350.50	7118.75	6378.11	18242.37						
351.50	8673.71	7896.23	26138.60						
352.50	10265.99	9469.85	35608.45						
353.50	11858.27	11062.13	46670.58						

# Stage - Discharge Table

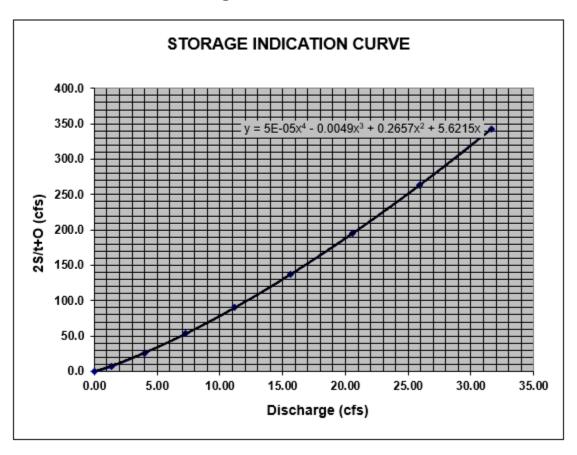
The following Stage Discharge Table is provided, based on the grading plan contained in the Civil Plans. The discharge structure planned for this facility is shown later in this report.

TYPE 2

Stage - Discharge for Rectangular Weir								
FL Discharge	Elevation	Increment	Top of Basin					
345.50	345.50	1.00	353.50					

04	11l (11)	Weir Length	A (A)	Orifice Coefficient	V-1:+-	Dih (0
Stage	Head (H)	(L)	Area (A)	(C)	Velocity	Discharge (Q
msl	ft	ft	sf		ft/s	cfs
345.50	0.00	0.42	0.00	3.33	0.00	0.00
346.50	1.00	0.42	0.42	3.33	3.33	1.40
347.50	2.00	0.42	0.84	3.33	4.71	3.96
348.50	3.00	0.42	1.26	3.33	5.77	7.27
349.50	4.00	0.42	1.68	3.33	6.66	11.19
350.50	5.00	0.42	2.10	3.33	7.45	15.64
351.50	6.00	0.42	2.52	3.33	8.16	20.56
352.50	7.00	0.42	2.94	3.33	8.81	25.90
353.50	8.00	0.42	3.36	3.33	9.42	31.65

#### **Storage Indication Curve**



### **Alternate Routing Time**

The following spreadsheets represent the Hydrograph Routing for the various storm events. In each case, the Routing Storm Duration time was adjusted to provide the maximum storage required. Also, runoff coefficients C have been adjusted for each storm event:

Storm Event	Pre C	Post C
2	0.41	0.47
5	0.44	0.50
10	0.47	0.53
25	0.52	0.58
50	0.55	0.61
100	0.59	0.66

Coefficients for Storage Indication Curve from Chart								
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx					
0.0001	-0.0049	0.2657	5.6215					

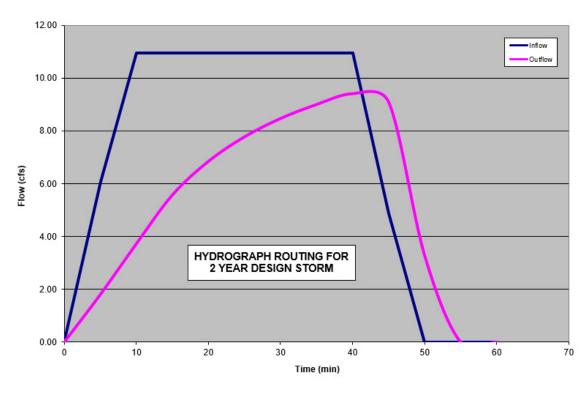
#### **HYDROGRAPH ROUTING FOR 2 YEAR DESIGN STORM**

**Routing Storm Duration** 

20	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	15.97	0	15.973	0	0	15.972	0.001
5	8.87	24.85	10.876	35.723	2.548	2013.7	35.724	-0.001
10	15.97	31.95	25.334	57.280	5.194	4579.3	57.280	0.000
15	15.97	31.95	41.818	73.764	7.731	7432.4	73.764	-0.001
20	15.97	23.07	54.737	77.809	9.513	9637.5	77.810	-0.001
25	7.10	7.10	57.939	65.038	9.935	10181.1	8.503	56.535
30	0.00	0.00	62.199	62.199	1.520	9527.8	0.000	62.199
35	0.00	0.00	50.999	50.999	0.000	9329.8	0.000	50.999
40	0.00	0.00	51.199	51.199	0.000	7649.8	0.000	51.199
45	0.00	0.00	51.399	51.399	0.000	7679.8	0.000	51.399
50	0.00	0.00	51.599	51.599	0.000	7709.8	0.000	51.599
55	0.00	0.00	51.799	51.799	0.000	7739.8	0.000	51.799
60	0.00	0.00	51.999	51.999	0.000	7769.8	0.000	51.999

Actual Maximum Storage needed is 10181.1 cubic feet
Maximum Storage required is achieved at an elev. = 349.32
Maximum Allowable (undeveloped) Discharge is 11.99 cfs
Maximum Discharge for the above storm is 9.93 cfs

#### **DETENTION HYDROGRAPH**



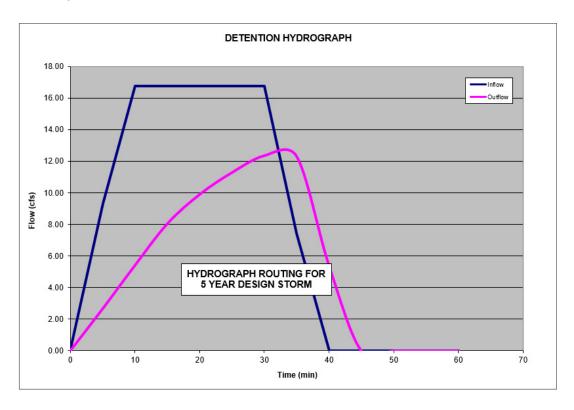
I	Coefficients	for Storage In	dication Curve	from Chart
	$Ax^4$	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
	0.0001	-0.0049	0.2657	5.6215

#### **HYDROGRAPH ROUTING FOR 5 YEAR DESIGN STORM**

Routing Storm Duration

30	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_{1}+I_{2}$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	16.75	0	16.750	0	0	16.749	0.001
5	9.31	26.06	11.428	37.484	2.661	2113.4	37.485	-0.001
10	16.75	33.50	26.658	60.157	5.413	4810.6	60.158	-0.001
15	16.75	33.50	44.056	77.555	8.051	7816.0	77.555	0.001
20	16.75	33.50	57.739	91.238	9.908	10147.0	91.236	0.002
25	16.75	33.50	68.648	102.147	11.295	11991.4	102.146	0.001
30	16.75	24.19	77.420	101.614	12.364	13467.5	101.615	-0.001
35	7.44	7.44	76.989	84.434	12.312	13395.2	36.484	47.950
40	0.00	0.00	73.856	73.856	5.389	11856.7	0.000	73.856
45	0.00	0.00	74.056	74.056	0.000	11078.4	0.000	74.056
50	0.00	0.00	74.256	74.256	0.000	11108.4	0.000	74.256
55	0.00	0.00	74.456	74.456	0.000	11138.4	0.000	74.456
60	0.00	0.00	74.656	74.656	0.000	11168.4	0.000	74.656

Actual Maximum Storage needed is 13467.5 cubic feet
Maximum Storage required is achieved at an elev. = 349.89
Maximum Allowable (undeveloped) Discharge is 14.9 cfs
Maximum Discharge for the above storm is 12.36 cfs



Coefficients	for Storage In	dication Curve	from Chart
$Ax^4$	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
0.0001	-0.0049	0.2657	5.6215

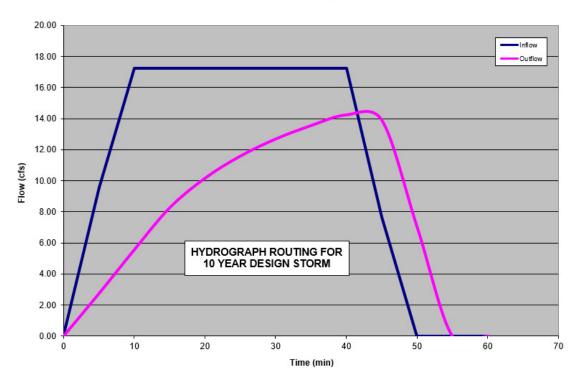
#### HYDROGRAPH ROUTING FOR 10 YEAR DESIGN STORM

**Routing Storm Duration** 

40	minutes							
	 1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 -
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	17.24	0	17.240	0	0	17.239	0.00
5	9.58	26.82	11.778	38.596	2.731	2176.3	38.597	-0.00
10	17.24	34.48	27.496	61.977	5.550	4956.9	61.976	0.00
15	17.24	34.48	45.475	79.956	8.251	8058.9	79.956	0.00
20	17.24	34.48	59.644	94.124	10.156	10469.9	94.123	0.00
25	17.24	34.48	70.962	105.442	11.581	12381.4	105.442	0.00
30	17.24	34.48	80.081	114.561	12.681	13914.2	114.560	0.00
35	17.24	34.48	87.472	121.953	13.544	15152.5	121.953	0.00
40	17.24	24.90	93.489	118.391	14.232	16158.1	118.390	0.00
45	7.66	7.66	90.587	98.249	13.902	15673.3	50.238	48.01
50	0.00	0.00	84.384	84.384	7.032	13682.5	0.000	84.38
55	0.00	0.00	84.584	84.584	0.000	12657.6	0.000	84.58
60	0.00	0.00	84.784	84.784	0.000	12687.6	0.000	84.78

Actual Maximum Storage needed is 16158.1 cubic feet
Maximum Storage required is achieved at an elev. = 350.25
Maximum Allowable (undeveloped) Discharge is 17.36 cfs
Maximum Discharge for the above storm is 14.23 cfs

#### **DETENTION HYDROGRAPH**



Coefficients	for Storage In	dication Curve	from Chart
$Ax^4$	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
0.0001	-0.0049	0.2657	5.6215

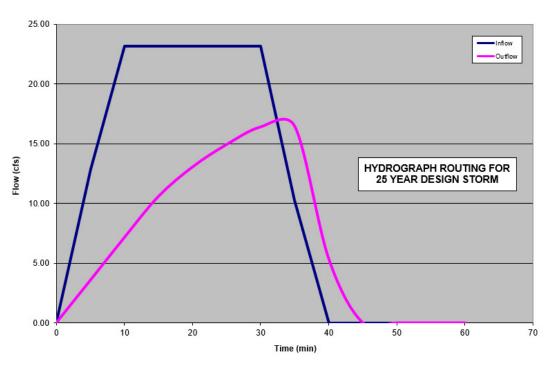
#### **HYDROGRAPH ROUTING FOR 25 YEAR DESIGN STORM**

**Routing Storm Duration** 

30	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	$S_2$	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	23.16	0	23.158	0	0	23.159	-0.00
5	12.87	36.02	16.041	52.065	3.559	2939.9	52.066	-0.001
10	23.16	46.32	37.780	84.097	7.142	6738.4	84.098	-0.00
15	23.16	46.32	62.939	109.256	10.579	11027.7	109.256	0.000
20	23.16	46.32	83.168	129.485	13.044	14431.8	129.484	0.00
25	23.16	46.32	99.641	145.958	14.922	17184.4	145.957	0.001
30	23.16	33.45	113.166	146.617	16.396	19434.3	146.616	0.001
35	10.29	10.29	113.708	124.001	16.454	19524.4	36.239	87.762
40	0.00	0.00	113.484	113.484	5.359	17796.3	0.000	113.484
45	0.00	0.00	113.684	113.684	0.000	17022.6	0.000	113.684
50	0.00	0.00	113.884	113.884	0.000	17052.6	0.000	113.884
55	0.00	0.00	114.084	114.084	0.000	17082.6	0.000	114.084
60	0.00	0.00	114.284	114.284	0.000	17112.6	0.000	114.284

Actual Maximum Storage needed is 19524.4 cubic feet
Maximum Storage required is achieved at an elev. = 350.65
Maximum Allowable (undeveloped) Discharge is 19.53 cfs
Maximum Discharge for the above storm is 16.45 cfs

#### DETENTION HYDROGRAPH



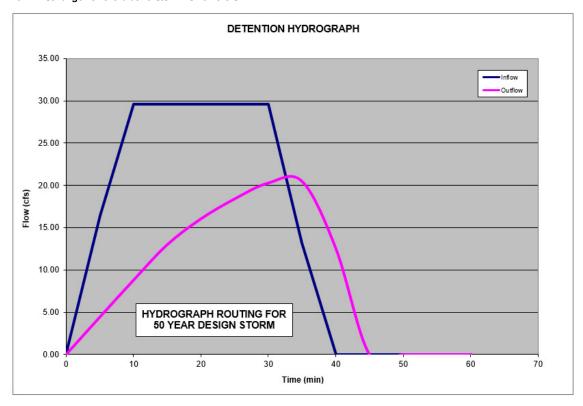
Coefficients	for Storage In	dication Curve	from Chart
Ax <sup>4</sup>	Bx <sup>3</sup>	Cx <sup>2</sup>	Dx
0.0001	-0.0049	0.2657	5.6215

#### **HYDROGRAPH ROUTING FOR 50 YEAR DESIGN STORM**

**Routing Storm Duration** 

30	30 minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	l <sub>1</sub> +l <sub>2</sub>	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	29.62	0	29.616	0	0	29.615	0.001
5	16.45	46.07	20.781	66.850	4.417	3779.8	66.850	0.000
10	29.62	59.23	49.291	108.522	8.779	8710.6	108.523	-0.001
15	29.62	59.23	82.573	141.804	12.974	14332.1	141.804	0.000
20	29.62	59.23	109.747	168.978	16.029	18866.3	168.978	0.000
25	29.62	59.23	132.202	191.433	18.388	22588.5	191.434	0.000
30	29.62	42.78	150.904	193.682	20.265	25675.3	193.683	-0.001
35	13.16	13.16	152.783	165.945	20.449	25984.8	102.860	63.085
40	0.00	0.00	141.080	141.080	12.532	23011.9	0.000	141.080
45	0.00	0.00	141.280	141.280	0.000	21162.0	0.000	141.280
50	0.00	0.00	141.480	141.480	0.000	21192.0	0.000	141.480
55	0.00	0.00	141.680	141.680	0.000	21222.0	0.000	141.680
60	0.00	0.00	141.880	141.880	0.000	21252.0	0.000	141.880

Actual Maximum Storage needed is 25984.8 cubic feet
Maximum Storage required is achieved at an elev. = 351.37
Maximum Allowable (undeveloped) Discharge is 25.68 cfs
Maximum Discharge for the above storm is 20.45 cfs



I	Coefficients	for Storage In	dication Curve	from Chart
	Ax <sup>4</sup>	$Bx^3$	Cx <sup>2</sup>	Dx
	0.0001	-0.0049	0.2657	5.6215

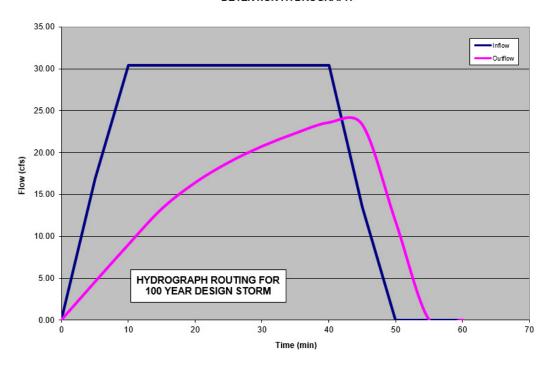
#### HYDROGRAPH ROUTING FOR 100 YEAR DESIGN STORM

**Routing Storm Duration** 

40	minutes							
	1	2	3	4	5	6	7	8
Time	I <sub>1</sub>	$I_1 + I_2$	2S <sub>1</sub> /t-Q <sub>1</sub>	2S <sub>2</sub> /t+Q <sub>2</sub>	$Q_2$	S <sub>2</sub>	2S/t-Q	Col 4 - 7
min	cfs	cfs	cfs	cfs	cfs	cf	from eqn.	
0	0.00	30.44	0	30.441	0	0	30.440	0.001
5	16.91	47.35	21.393	68.745	4.524	3887.5	68.746	-0.001
10	30.44	60.88	50.780	111.662	8.983	8964.4	111.661	0.001
15	30.44	60.88	85.119	146.000	13.272	14758.5	146.001	-0.001
20	30.44	60.88	113.200	174.082	16.400	19440.0	174.083	-0.001
25	30.44	60.88	136.442	197.324	18.820	23289.3	197.323	0.001
30	30.44	60.88	155.829	216.711	20.747	26486.5	216.710	0.001
35	30.44	60.88	172.091	232.972	22.310	29160.1	232.973	-0.001
40	30.44	43.97	185.788	229.759	23.592	31407.1	229.758	0.001
45	13.53	13.53	183.077	196.607	23.341	30962.7	94.375	102.232
50	0.00	0.00	173.395	173.395	11.706	27735.1	0.000	173.395
55	0.00	0.00	173.595	173.595	0.000	26009.2	0.000	173.595
60	0.00	0.00	173.795	173.795	0.000	26039.2	0.000	173.795

Actual Maximum Storage needed is 31407.1 cubic feet
Maximum Storage required is achieved at an elev. = 352.03
Maximum Allowable (undeveloped) Discharge is 29.36 cfs
Maximum Discharge for the above storm is 23.59 cfs

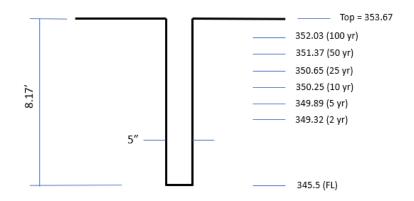
#### DETENTION HYDROGRAPH



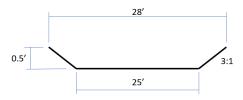
# **Summary – Detention**

Storm Event	Volume Needed (cf)	WSE	Max Discharge Allowed (cfs)	Max Discharge Model (cfs)
2	10181.1	349.32	11.99	9.93
5	13467.5	349.89	14.90	12.36
10	16158.1	350.25	17.36	14.23
25	19524.4	350.65	19.53	16.45
50	25984.8	351.37	25.68	20.45
100	31407.1	352.03	29.36	23.59

# **Discharge Structure Detail**



#### **Overflow Structure Detail**



 $Q = (1.49/n)(A)(R^2/3)(S^0.5)$ 

Q = (1.49/0.025)(13.25)(0.60)(0.1) = 47.38 cfs

Required Capacity = 23.59 cfs (2) = 47.18 cfs

# **Study Point Summary (25 yr Storm)**



Study Point	Pre Construction	Post Construction	Post Construction	Change - Pre to Post
	Q	Q (no detention)	Q (with detention)	(with detention)
	(cfs)	(cfs)	(cfs)	(cfs)
Α	12.88	16.81	16.81	3.93
В	10.53	0	0	-10.53
С	11.01	0	0	-11.01
<u>D</u>	<u>17.74</u>	<u>38.08</u>	<u>16.45</u>	<u>-1.29</u>
TOTAL	52.16	54.89	33.26	-18.9

<sup>\*</sup> Existing culvert originating at the Junction Box near the NE corner of Hurricane Gardens has adequate capacity to accept this slight increase in flow.

# **Downstream Considerations**

The discharge from the proposed Detention Facility will enter into an existing ditch that drains to the West, into Hurricane Lake, Phase 3. The ditch exists between Lots 47 and 48 of said development (based on Saline County GIS map). A 54" CMP (Helical) culvert exists under Worth Ave, at a grade of 0.7% (as shot in the field). Using an n of 0.012, the capacity of this culvert is computed at 183.65 cfs at d/D of 0.85 (velocity = 12.75 fps). It should be noted that the estimated post construction discharge is 1.29 cfs less than the estimated existing runoff from the same area. Therefore, this development should not have a negative impact on the downstream properties.



Source: Saline County GIS

# **Engineering Certification**

I, Tim Lemons, Arkansas Registered Professional Engineer No. 7373, hereby certify that the drainage reports, and calculations contained in this report, have been prepared in accordance with sound engineering practice and principles, and based on best known available data. Improvements as outlined in this report and depicted on the preliminary plat and design drawings should not increase the risk of endangerment to life or have negative impacts on adjacent or downstream property or watersheds.



Timothy B. Lemons, PE Arkansas Professional Engineer, #7373

# **Appendix**

Clara -	. O E0/ -	- 0 013						
siope =	= 0.5%, r	n = 0.012						
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)	·	(ft)	(sf)					(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.00500	0.0707	0.00
1	0.030	0.03	0.02	0.01	0.06	0.00500	0.0707	0.01
1.5	0.030	0.05	0.03	0.02	0.08	0.00500	0.0707	0.02
2	0.030	0.06	0.06	0.03	0.10	0.00500	0.0707	0.05
2.5	0.030	0.08	0.09	0.04	0.11	0.00500	0.0707	0.09
3	0.030	0.09	0.14	0.04	0.13	0.00500	0.0707	0.15
3.5	0.030	0.11	0.18	0.05	0.14	0.00500	0.0707	0.22
4	0.030	0.12	0.24	0.06	0.15	0.00500	0.0707	0.32
4.5	0.030	0.14	0.30	0.07	0.16	0.00500	0.0707	0.44
5	0.030	0.15	0.38	0.07	0.18	0.00500	0.0707	0.58
5.5	0.030	0.17	0.45	0.08	0.19	0.00500	0.0707	0.75
6	0.030	0.18	0.54	0.09	0.20	0.00500	0.0707	0.94
6.5	0.030	0.20	0.63	0.10	0.21	0.00500	0.0707	1.17
7	0.030	0.21	0.74	0.10	0.22	0.00500	0.0707	1.43
7.5	0.030	0.23	0.84	0.11	0.23	0.00500	0.0707	1.71
8.5	0.030	0.26	1.08	0.13	0.25	0.00500	0.0707	2.39
9	0.030	0.27	1.22	0.13	0.26	0.00500	0.0707	2.79
9.5	0.030	0.29	1.35	0.14	0.27	0.00500	0.0707	3.22
10	0.030	0.30	1.50	0.15	0.28	0.00500	0.0707	3.69
10.5	0.030	0.32	1.65	0.16	0.29	0.00500	0.0707	4.21
11	0.030	0.33	1.82	0.16	0.30	0.00500	0.0707	4.76
11.5	0.030	0.35	1.98	0.17	0.31	0.00500	0.0707	5.36
12	0.030	0.36	2.16	0.18	0.32	0.00500	0.0707	6.01
12.5	0.030	0.38	2.34	0.19	0.33	0.00500	0.0707	6.70
13	0.030	0.39	2.54	0.19	0.33	0.00500	0.0707	7.44

Slope =	= 1.50%	n = 0.012	2					
J. 0 P C	,	. 0.02.	_					
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)		(ft)	(sf)					(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.01500	0.1225	0.00
1	0.030	0.03	0.02	0.01	0.06	0.01500	0.1225	0.01
1.5	0.030	0.05	0.03	0.02	0.08	0.01500	0.1225	0.04
2	0.030	0.06	0.06	0.03	0.10	0.01500	0.1225	0.09
2.5	0.030	0.08	0.09	0.04	0.11	0.01500	0.1225	0.16
3	0.030	0.09	0.14	0.04	0.13	0.01500	0.1225	0.26
3.5	0.030	0.11	0.18	0.05	0.14	0.01500	0.1225	0.39
4	0.030	0.12	0.24	0.06	0.15	0.01500	0.1225	0.55
4.5	0.030	0.14	0.30	0.07	0.16	0.01500	0.1225	0.76
5	0.030	0.15	0.38	0.07	0.18	0.01500	0.1225	1.01
5.5	0.030	0.17	0.45	0.08	0.19	0.01500	0.1225	1.30
6	0.030	0.18	0.54	0.09	0.20	0.01500	0.1225	1.64
6.5	0.030	0.20	0.63	0.10	0.21	0.01500	0.1225	2.03
7	0.030	0.21	0.74	0.10	0.22	0.01500	0.1225	2.47
7.5	0.030	0.23	0.84	0.11	0.23	0.01500	0.1225	2.97
8.5	0.030	0.26	1.08	0.13	0.25	0.01500	0.1225	4.15
9	0.030	0.27	1.22	0.13	0.26	0.01500	0.1225	4.83
9.5	0.030	0.29	1.35	0.14	0.27	0.01500	0.1225	5.58
10	0.030	0.30	1.50	0.15	0.28	0.01500	0.1225	6.40
10.5	0.030	0.32	1.65	0.16	0.29	0.01500	0.1225	7.29
11	0.030	0.33	1.82	0.16	0.30	0.01500	0.1225	8.25
11.5	0.030	0.35	1.98	0.17	0.31	0.01500	0.1225	9.29
12	0.030	0.36	2.16	0.18	0.32	0.01500	0.1225	10.41
12.5	0.030	0.38	2.34	0.19	0.33	0.01500	0.1225	11.61
13	0.030	0.39	2.54	0.19	0.33	0.01500	0.1225	12.89

		ITY OF ST		Z/ BCT	.U DC			
Slope =	= 2.67%,	n = 0.012	2					
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)	Siope	(ft)	(sf)	I N	11. 2/3	3	3-1/2	(cfs)
(10)		(10)	(31)					(013)
0.5	0.030	0.02	0.00	0.01	0.04	0.02670	0.1634	0.00
1	0.030	0.03	0.02	0.01	0.06	0.02670	0.1634	0.02
1.5	0.030	0.05	0.03	0.02	0.08	0.02670	0.1634	0.05
2	0.030	0.06	0.06	0.03	0.10	0.02670	0.1634	0.12
2.5	0.030	0.08	0.09	0.04	0.11	0.02670	0.1634	0.21
3	0.030	0.09	0.14	0.04	0.13	0.02670	0.1634	0.34
3.5	0.030	0.11	0.18	0.05	0.14	0.02670	0.1634	0.52
4	0.030	0.12	0.24	0.06	0.15	0.02670	0.1634	0.74
4.5	0.030	0.14	0.30	0.07	0.16	0.02670	0.1634	1.01
5	0.030	0.15	0.38	0.07	0.18	0.02670	0.1634	1.34
5.5	0.030	0.17	0.45	0.08	0.19	0.02670	0.1634	1.73
6	0.030	0.18	0.54	0.09	0.20	0.02670	0.1634	2.18
6.5	0.030	0.20	0.63	0.10	0.21	0.02670	0.1634	2.70
7	0.030	0.21	0.74	0.10	0.22	0.02670	0.1634	3.29
7.5	0.030	0.23	0.84	0.11	0.23	0.02670	0.1634	3.96
8.5	0.030	0.26	1.08	0.13	0.25	0.02670	0.1634	5.53
9	0.030	0.27	1.22	0.13	0.26	0.02670	0.1634	6.44
9.5	0.030	0.29	1.35	0.14	0.27	0.02670	0.1634	7.44
10	0.030	0.30	1.50	0.15	0.28	0.02670	0.1634	8.53
10.5	0.030	0.32	1.65	0.16	0.29	0.02670	0.1634	9.72
11	0.030	0.33	1.82	0.16	0.30	0.02670	0.1634	11.01
11.5	0.030	0.35	1.98	0.17	0.31	0.02670	0.1634	12.40
12	0.030	0.36	2.16	0.18	0.32	0.02670	0.1634	13.89
12.5	0.030	0.38	2.34	0.19	0.33	0.02670	0.1634	15.49
13	0.030	0.39	2.54	0.19	0.33	0.02670	0.1634	17.20

		ITY OF ST						
oope =	4.88%,	n = 0.012						
Width	Slope	Height	Area	R	R^2/3	S	S^1/2	Q
(ft)		(ft)	(sf)		•		-	(cfs)
0.5	0.030	0.02	0.00	0.01	0.04	0.04880	0.2209	0.00
1	0.030	0.03	0.02	0.01	0.06	0.04880	0.2209	0.02
1.5	0.030	0.05	0.03	0.02	0.08	0.04880	0.2209	0.07
2	0.030	0.06	0.06	0.03	0.10	0.04880	0.2209	0.16
2.5	0.030	0.08	0.09	0.04	0.11	0.04880	0.2209	0.28
3	0.030	0.09	0.14	0.04	0.13	0.04880	0.2209	0.46
3.5	0.030	0.11	0.18	0.05	0.14	0.04880	0.2209	0.70
4	0.030	0.12	0.24	0.06	0.15	0.04880	0.2209	1.00
4.5	0.030	0.14	0.30	0.07	0.16	0.04880	0.2209	1.37
5	0.030	0.15	0.38	0.07	0.18	0.04880	0.2209	1.81
5.5	0.030	0.17	0.45	0.08	0.19	0.04880	0.2209	2.34
6	0.030	0.18	0.54	0.09	0.20	0.04880	0.2209	2.95
6.5	0.030	0.20	0.63	0.10	0.21	0.04880	0.2209	3.65
7	0.030	0.21	0.74	0.10	0.22	0.04880	0.2209	4.45
7.5	0.030	0.23	0.84	0.11	0.23	0.04880	0.2209	5.35
8.5	0.030	0.26	1.08	0.13	0.25	0.04880	0.2209	7.48
9	0.030	0.27	1.22	0.13	0.26	0.04880	0.2209	8.71
9.5	0.030	0.29	1.35	0.14	0.27	0.04880	0.2209	10.06
10	0.030	0.30	1.50	0.15	0.28	0.04880	0.2209	11.54
10.5	0.030	0.32	1.65	0.16	0.29	0.04880	0.2209	13.14
11	0.030	0.33	1.82	0.16	0.30	0.04880	0.2209	14.88
11.5	0.030	0.35	1.98	0.17	0.31	0.04880	0.2209	16.76
12	0.030	0.36	2.16	0.18	0.32	0.04880	0.2209	18.77
12.5	0.030	0.38	2.34	0.19	0.33	0.04880	0.2209	20.94
13	0.030	0.39	2.54	0.19	0.33	0.04880	0.2209	23.25



October 21, 2024

Mr. Colton Leonard, City Planner City of Bryant, Arkansas Community Development 210 SW 3<sup>rd</sup> Street Bryant, Arkansas 72022

Re: Preliminary Plat

3927 Springhill Road, Bryant, AR

Parcel # 840-11855-000

Dear Mr. Leonard:

Enclosed you will find the revised Civil Plans, and Drainage Report as pertaining to the referenced project. A brief summary of the revisions are as follows. Please review the attached revised plans, and include this project on the agenda of the next available City of Bryant Planning Commission Meeting.

#### **Public Works**

- 1. Discuss where the sewer will tie in. Connection is planned within the Hurricane Gardens development. See plans.
- 2. Will roads be Public or Private? Public.
- 3. Discuss Half Street Improvements. Half Street Improvements have been added to the revised plans as per the City's Master Plan.
- 4. Core Sample Test will be required per Bryant Minimum Street Specifications. The test results shall be provided to the city upon receipt.
- **5.** ADA Compliant Ramps will be required at Crosswalk. **References to this requirement have been** added to the revised plans.
- **6.** Additional "No Parking" signs will be required beyond the two that are listed. **See revised plans** showing the placement of such signs.

#### Stormwater

1. Discuss downstream drainage issues into Hurricane Gardens Subdivision? Since the original submittal, we have added a swale along the South property line of the subject tract, which is near

the North subdivision line of Hurricane Gardens. This is shown on the revised plan and is taken into account with the revised Drainage Report. With the construction of the street within Hillcrest Addition, along with the swale along the South, the amount of discharge into the rear of the lots of Hurricane Gardens will be tremendously reduced, and in most cases, completely removed.

- 2. Discuss Storm Plans in detail (Piping, detention, retention, street inlets).
  - a. As the City is aware, the property to the North of Hurricane Gardens drains directly into the rear of the lots along the North side of that development. The source of this stormwater is not only that which falls on the vacant land of the proposed Hillcrest Addition, but also a large area located to the North of the proposed Hillcrest Addition. In short, the Hurricane Gardens area is receiving approximately 10 acres of runoff into the rear of said lots. There are two items planned that should help the residents of Hurricane Gardens. First, the construction of the proposed street in the Hillcrest Addition development will help divert the stormwater away from the Hurricane Gardens lots by diverting it to the proposed detention pond near the Southwest corner of Hillcrest. Second, the addition of the swale along the South line of Hillcrest should catch the stormwater that will be falling on the rear of the lots in Hillcrest, to the same detention pond.
  - b. The piping and inlets are design to accommodate a 25 year storm as opposed to the required 10 year storm. Again, attention is called to the Revised Drainage Report.
- **3.** Detention basin outflow pipe is shown to be ADS. It is required to be RCP. **This has been revised as requested.**

## **Engineering**

- 1. Verify drainage area. Topography and eye witness accounts indicate the site receives runoff from north and east off-site and Springhill road. *This has been verified*.
- 2. 0890-DRN-03.PDF
- **a.** This off-site drainage plan shows the drainage basins that exist are apparently based upon the contours from Bryant's GIS, even though there is no reference to the source of the base map and contours. **Information added to the Drainage Report.**
- b. There does not appear to be any basins delineated which extend to the south property line of the proposed subdivision. Provide a map showing the pre-development basins for the site, with checkpoints at all locations where flows leave the site. Information and maps added to the Drainage Report.
- 3. 0890-PLN-02.PDF
- a. On sheet 1, some of the lot dimensions are obscured on the drawing. This has been revised.
- b. On sheet 2:
- i. the curb and gutter detail does not match the detail show in the City of Bryant's standard curb and gutter section, Detail 7; *This has been revised.*
- ii. The typical street section does not match Detail 1 of the City of Bryant's typical section for Local 1 / Residential Streets; This has been revised.
- *iii*. The pavement structure detail shown does not match the typical street section, see 3.b.ii. above. *This* has been revised.
  - c. On sheet 3:
- i. The grading plan shows that grades will continue to slope south from the south curb and gutter on the street, unlike shown in the drainage calculations (see section 4 below). Grading Plan has been revised.

- ii. Significant stormwater is being allowed to drain off of the site to the south, it is recommended that the engineer look at diverting flow to the detention pond. A swale has been added along the South property line to assist in diverting flow away from homes within Hurricane Gardens. See revised plans.
- *iii.* Will a separate drainage plan be developed for the plans? Profiles for the storm drainage? *Drainage profiles have been added to the plans.*
- iv. How will the discharge to Springhill Road be detained so that there is no increase in runoff from that part of the project? Due to the relatively small area flowing into the culvert system near the Southeast corner of the proposed development, no detention is being provided. However, the existing culvert does appear to have the capacity to accept the small increase in flow. This is further explained in the Drainage Report under the "Culvert Sizing Section (Junc Box 3)".
  - d. On sheet 4:
- i. Include a trickle channel in the pond; Added.
- ii. Include an emergency overflow for the pond, designed for the 100-year flow. This overflow must be 1-ft below the top of the levee. *Added as applicable (see comment vii below).*
- *iii.* Verify that the slopes inside and outside of the pond are no steeper than 3 horizontal : 1 vertical. *All* slopes have been verified.
- *iv.* The outfall structure detail of the pond shown on the drawing is not labeled or titled. Show slopes, elevations, etc. *Information added as requested*.
- v. Provide solid sodding inside of the pond. A note pertaining to this item has been added to the plans.
- vi. How far will the closest building be to the pond? Approximately 50 feet.
- vii. The top of the levee on the detention pond must be 2-ft above the outfall box, include 1-ft of freeboard, and be 1-ft higher than the 100-year elevation inside of the pond. Based on our present model, we can only provide 18" of the requested 2'. We ask that the City grant a waiver on the 6" difference.
- viii. What downstream scour protection will there be below the outfall pipe? Rip rap is planned for the discharge culvert from the pond.
- ix. What checks have been performed in the drain to the southwest? Verify that the flows will not exceed the current flows in this area. See Drainage Report under "Downstream Considerations".
- x. Provide Scour protection from the inflow pipe on the east end of the pond. A concrete trickle channel has been added to the end of the inflow FES.
  - e. On sheet 5:
- *i.* The main water line must be at least 8" up to the last fire hydrant, see city specifications. *This has been revised.*
- *ii.* The last fire hydrant shown on the west side of the cul-de-sac should be moved to the east side of the cul-de-sac. *Revised as requested.* 
  - 4. Drainage Calculations:
  - **a.** For the runoff coefficient calculations on pages 5 and 6, please explain which basins A1, A2, A3, and A4 reflect. What about Basins B1 thru D3 and A0 thru Do2? **We have completely revised the attached Drainage Report for clarity. Please review.**
  - **b.** Each return storm has it's own C-factor. Show the C-factor used for each of the return storms, on each basin. **This was shown in the previous revised report.**
  - c. Detention pond design volume must be increased by 25% as a safety factor. At the 25 year storm elevation (in the pond) the volume is 21,300.7 cf. At the 100 year storm elevation, the volume is 31,596.5 cf. That is above the 25% safety factor.

- d. The emergency overflow spillway must be designed for the 100-year storm + 50% for blockage. Emergency spillway has the required capacity of 44.22 cfs. See Drainage Report "Overflow Structure Detail", sheet 33.
- **e.** The map on page 9 does not show the pre-development basins, including the current discharge locations from the site. **Study Points have been added to all maps.**
- f. Determine pre-development basins from the same discharge points for both pre-development and post-development conditions. The comparison between Pre and Post flowrates are shown near the end of the Drainage Report under "Study Point Summary".
- **g.** The basins shown on the map on page 10 does not reflect what the grading plan shows, see sheet 3 in the plans. It shows drainage of half of the lots going to the street, when the grading plan shows that flows will go to the south. **This has been corrected. See revised Drainage Report and attached Maps.**
- h. Show check points for each basin so calculations can be followed. Check points have been added to the maps within the Drainage Report.
- i. Show the hydraulic grade calculations for all of the storm drainage on the project (see section 600 in the stormwater manual). *This has been added to the Drainage Report.*
- Adjust drainage calculations for all flows for a 28-ft street instead of a 27-ft street. Revised.
- **k.** Show calculations for emergency spillway (include 50% blockage). **See previous comment and response.**
- I. Are the time of concentration calculations on pages 16 and 17 showing that there is the same velocity for all basins? Which basins do these graphs apply to for the pond? This is a comprehensive analysis using the entire watershed. However, individual tc values have been computed for each pre construction watershed (see revised Drainage Report).
- m. On page 15 it refers to the C-factor for the detention facility was shown on pages 5 and 6 but the C-factor is different for each storm event, and that is not reflected on pages 5 and 6. This was revised in an earlier submittal (See sheets 6 and 7 of the Drainage Report).
- n. For the detention pond calculations, what basin(s) did you use for the pre- and post-development peak flows? The areas behind the proposed houses in this new development were not included in the Detention computations. However, we have added a sod swale along the South of this development that will assist in sending most, if not all of the area to the Detention facility. See revised plans.
- o. Sheet 4 in the plans shows a detail for a box with a slotted weir topped with a 5" high rectangular weir. Please verify that calculations reflect the correct weir type. Yes the calculations are based on this type of weir.
- **p.** Refer to section 1000.4.3 of the stormwater manual for multi-stage outlet design considerations. **After reviewing this section, it is our opinion that the design does meet this consideration.**
- q. Refer to section 1000.5.6 of the stormwater manual for configuration of the outlet structure. *After reviewing this section, it is our opinion that the design does meet said section.*
- r. Note allowable computer software in section 600.6 of the stormwater manual. Our program is based on the City of Rogers Drainage Manual which has been used by basically all municipalities in Northwest Arkansas, and is considered an acceptable method.

#### **Com Dev**

1. Cul-de-sac turnarounds must have a 50ft radius. Currently the plans show 49' to BOC. *This has been revised as requested.* 

- 2. According to Subdivision Code, Cul-de-sac streets or courts designed to have one end permanently closed shall be no more than 550' long. This will have to be met or a modification from the subdivision code for a waiver on this requirement will have to be requested. Considering that all properties adjacent to this development have been developed, we formally ask for this waiver.
- **3.** Half-Street improvements to Springhill are required as part of this development. Springhill is designated as a minor arterial with a trail along the East Side. **Plans have been modified to show this**.
- **4.** Typical street cross section shown on page 3 of plans does not meet our street specifications. City Street specification for local road shown below. **This has been corrected. Please see attached revised plans.**
- 5. Will this street be privately owned/maintained? Street shall be public.
- 6. Discuss stormwater and outfall of detention pond area. See previous responses in this letter.
- 7. Preliminary Plat application fees required to be paid \$664. *I will inform the owner.*

Please let me know if you need anything additional.

Sincerely,

Tim Lemons, PE



## **Rezoning Application**

Applicants are advised to read the Amendments section of Bryant Zoning Code prior to completing and signing this form. The Zoning Code is available at <a href="https://www.cityofbryant.com">www.cityofbryant.com</a> under the Planning and Community Development tab.

Date: 10	124	
Applicant or Des	signee:	Property Owner (If different from Applicant):
Name FINIC	y + company	Name Danny + Donna Anderson Trustees With Address 198 w Lawson Fd. Alexander Trus
Address P.O. P	xox 10, Bygant	Address 198 W LAWSON FO. Alexander Trus
Phone <u>1701 - 1</u> 0	46-1300 n	Phone AP, 12002 - 9430
Email Address 24	uart @ finiey	Email Address
Property Inform	nacompany.cov	1
Address	200 en 100 en 10	
Parcel Number 🖇	40-10010-000	
Existing Zoning Cla		
Requested Zoning	Classification <u>C-3</u>	<del></del>
^	793 V	description, please attach in a legible typed format)
Application Su	bmission Checklist:	
	tating request of zoning cha be placed on the Planning C	ange from (Current Zoning) to (Requested Zoning) commission Agenda
□ Comple	ted Rezoning Application	
	ng Application Fee (\$40 fee and bound descriptions)	for lot and black descriptions or \$125 for acreage or
□ If some	one, other than the owner,	will be handling the zoning process, we will require a

letter from the owner of said property, giving him or her authority to do so.
Recent surveyed plat of the property including vicinity map
onal Requirements:
below <b>must be completed before the public hearing can occur</b> . Failure to provide notices in the llowing manners shall require delay of the public hearing until notice has been properly made.
Publication: Public Notice shall be published by the applicant at least one (1) time fifteen (15) days prior to the public hearing at which the rezoning application will be heard. Once published please provide a proof of publication to the Community Development office. (Sample notice attached below)
Posting of Property: The city shall provide signs to post on the property involved for the fifteen (15) consecutive days leading up to Public hearing. One (1) sign is required for every two hundred (200) feet of street frontage.
Notification of adjacent landowners: Applicant shall attempt to inform by certified letter, return receipt requested, all owners of land within three hundred (300) feet of any boundary of the subject property of the public hearing. (Sample letter attached below)
Certified list of property owners, all return receipts, and a copy of the notice shall be provided to the Community Development Department at least five (5) days prior to the public hearing.
that this is not an exhaustive guideline regarding the Conditional Use Permit Process.  Additional information is available in the Bryant Zoning Ordinance.
CAREFULLY BEFORE SIGNING
do hereby certify that all information contained within this application is correct. I further certify that the owner of the property authorizes this proposed application. I understand that I must with all City Codes that pertain to this project and that it is my responsibility to obtain all necessary permits as needed.

## **NOTICE OF PUBLIC HEARING**

A public hearing will l	oe held on Monday,	November	// at 6:00 P.M.
at the Bryant City Off	fice Complex, 210 Sout	thwest 3 <sup>∞</sup> Street, City	of Bryant, Saline
County, for the purpo	ose of public comment of	on a conditional use	request at the site of
Parcel #	+ 840-15010-00	<b>5</b> 0	(address).
A legal description of	this property can be o	btained by contacting	g the Bryant Department
of Community Develo	opment.		
	Chairn	ohnson nan Board of Zoning f Bryant	Adjustment

This notice is to be run in the legal notices section of the Saline Courier no less than 15 days prior to the public hearing.

## **SAMPLE LETTER**

Date		
Name		
Address		
RE: Rezoning Petition		
The property located at _		is being considered for
rezoning from	to	The property is more particularly described as
follows:		
	INSERT LEGAL	DESCRIPTION OF PROPERTY
An application has been fi	ilad with the City of	Bryant Planning Commission to rezone the property. As
		eld on Monday, 2021 at 6:00 PM in
the Boswell Community C	enter Courtroom, 2	10 SW 3 <sup>rd</sup> Street, Bryant, AR 72022.
Public comments will be a	accepted at that tim	e regarding this rezoning. Since you own property within
300 feet of the property in	n consideration, you	u have been sent this letter via certified mail as required by
city ordinance.		
Should you have any ques	stions regarding this	matter you may contact the City of Bryant at 501-943-
0857 or by contacting me	at	<u></u>
		ь'
Thank you for your consid	deration in this matt	ter.
Sincerely,		
Your Signature		
Vour Name		

#### LEGAL NOTICE

NOTICE IS HEREBY GIVEN THAT A PUBLIC HEARING WILL BE HELD ON MONDAY, NOVEMBER 11, 2024 AT 6:00 PM AT THE BRYANT CITY OFFICE COMPLEX, 210 SW 3RD ST., BRYANT, AR 72022 FOR THE PURPOSE OF PUBLIC COMMENT FOR REZONE APPROVAL ON BEHALF OF FINLEY & COMPANY OF THE 33 ACRE PROPERTY LOCATED ON THE EAST SIDE OF ALCOA RD. PARCEL #840-15010-000 LYING WEST OF MOUNT CARMEL RD., BRYANT, AR.. THE APPLICATION REQUESTS TO REZONE FROM IT'S CURRENT ZONING OF R-E TO C-3. FOR INFORMATION PLEASE CONTACT HOPE CONSULTING, INC. AT 501-315-2626.

Type of Instrument: Special Warranty Deed
Grantors: Danny Daryl Anderson and Donna Faye Anderson,
Husband and Wife
Grantee: Danny Anderson and Donna Anderson,
Trustees of the Anderson Living Trust,
dated March 4, 2019

This Instrument Prepared
Without Title Search of Survey By:
Nash Law Firm, P. A.
Attorneys at Law
103 Park Drive
Maumelle, AR 72113

After Recording Return To: Nash Law Firm, P. A. 103 Park Drive Maumelle, AR 72113



was filed on: 04/11/2019 11:25:51 AM Myka Bono Sample Saline County Circuit Clerk

I certify this instrument

Pages: 5 C GREER

#### SPECIAL WARRANTY DEED

#### KNOW ALL PERSONS BY THESE PRESENTS:

THAT, DANNY DARYL ANDERSON and DONNA FAYE ANDERSON, Husband and Wife, hereinafter GRANTORS, for and in consideration of the sum of Ten and 00/100 Dollars (\$10.00) and other good and valuable consideration in hand paid by DANNY ANDERSON and DONNA ANDERSON, Trustees of the ANDERSON LIVING TRUST, dated March 4, 2019, and any amendments thereto, hereinafter GRANTEE, the receipt and sufficiency of which is hereby acknowledged, do hereby grant, bargain, sell and convey all of their right, title, and interest unto the GRANTEE, and unto its successors and assigns forever, in and to the following described lands located in the County of Saline, State of Arkansas, to wit:

#### SEE EXHIBIT "A"

To have and to hold, unto the GRANTEE, and unto its successors and assigns forever, with all tenements, appurtenances and hereditaments thereunto belonging, retaining their homestead rights therein subject to the terms of the Trust referred herein.

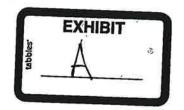
AND THE GRANTORS DO HEREBY COVENANT with the Grantee, except as above-noted, that at the time of the delivery of this Deed, the premises were free from all encumbrances made by it, and that it will warrant and defend the same against the lawful claims and demands of all persons claiming, by, through, or under it, but against none other.

In Witness Whereof I have hereunto set my hand this

day of March, 201

ONNA FAYE ANDERSON, Grantor

DANN DARYL ANDERSON Granter



### Tract I:

That part of the South half of the Northeast Quarter of Section 32, Township 1 South, Range 14 West, described as follows: Beginning at a point 377 feet East of the Southwest corner of the East half of the

Southwest Quarter of the Northeast Quarter of said Section 32 and run thence East 377 feet; thence North to the North line of said South half of said Northeast Quarter; thence West 377 feet; thence South to the point of beginning, consisting of 11 acres, more or less.

### Tract II:

The South half of the Southwest Quarter of Southwest Quarter consisting of 20 acres and part of the North half of the Southwest Quarter of Southwest Quarter described as follows: Beginning at the Southwest corner of said North half of the Southwest Quarter of the Southwest Quarter and thence run North 159 feet to the South line of the First Electric Cooperative Corporation lands and thence run East along the south lien of said First Electric Cooperative Corporation lands 1320 feet to the East boundary line of said North half of the Southwest Quarter of Southwest Quarter; thence South 159 feet to the Southeast corner of said North half of Southwest Quarter of Southwest Quarter; thence West 1320 feet to a point of beginning. And part of the Southeast Quarter of the Southwest Quarter described as follows: Beginning at the Southwest corner of said Southeast Quarter of Southwest Quarter and run thence North 819 feet to the South line of the First Electric Cooperative Corporation lands, thence East along the South side of said First Electric Cooperative Corporation lands, 195 feet; thence South 210 feet; thence East 446 feet to the West side of a public road as now located; thence South along the West side of said public road to the South line of said Southeast Quarter of Southwest Quarter; thence West to the point of beginning all said lands lying in Section 29, township 1 South, Range 14 West in Saline County, Arkansas and containing in the aggregate 33 acres, more or less.

#### LESS AND EXCEPT:

Part of the Southwest Quarter of the Southwest Quarter of Section 29, Township 1 South, Range 14 West, Saline County, Arkansas being more particularly described as follows: Commencing at a ¾ inch pipe used as the Southeast corner of the Southeast Quarter of the Southwest Quarter of Section 29; thence North 89 deg. 14 min. 12 sec. West along the South line thereof a distance of 1,333.88 feet to a point being used as the Southeast corner of the Southwest Quarter of the Southwest Quarter of Section 29; thence North 89 deg. 14 min. 12 sec. West along the South line thereof a distance of 1,235.55 feet to a

840-15010-000



point on the East right of way line of Alcoa Road as established by AHTD Job 061267 for the point of beginning: thence continuing North 89 deg. 14 min. 12 sec. West along said South line a distance of 30.02 feet to a point; thence continuing North 89 deg. 14 min. 12 sec. West along said South line a distance of 29.29 feet to a point on the East right of way line of Alcoa Road as established by AHTD Job C-62-4; thence north 3 deg. 03 min. 29 sec. East along said right of way line a distance of 255.81 feet to a point; thence North 1 deg. 52 min. 14 sec. East along said right of way line a distance of 562.25 feet to a point; thence South 88 deg. 49 min. 00 sec. East a distance of 92.83 feet to a point on the East right of way line of Alcoa Road as established by AHTD Job 061297; thence South 1 deg. 47 min. 55 sec. West along said right of way line a distance of 52.06 feet to point; thence South 22 deg. 04 min. 53 sec. West along said right of way line a distance of 49.04 feet to a point; thence South 60 deg. 50 min. 06 sec. West along said right of way line a distance of 34.99 feet to a point; thence South 28 deg. 31 min. 43 sec. West along said right of way line a distance of 48.91 feet to a point; thence South 1 deg. 47 min. 55 sec. West along said right of way line a distance of 179.31 feet to a point; thence South 1 deg. 03 min. 04 sec. West along said right of way line a distance of 150.17 feet to a point; thence South 2 deg. 17 min. 28 sec. West along said right of way line a distance of 288.04 feet to a point; thence South 34 deg. 18 min. 23 sec. East along said right of way line a distance of 50.34 feet to the Point of Beginning and containing 0.67 acres, more or less or 29,024 square feet, more or less.

## Condition:

Subject to the condition and the condition shall be a covenant that shall run with the land that said Danny Daryl Anderson and/or Donna Faye Anderson, their heirs and assigns may not, under any circumstances, permit the use, lease or purchase of the land by any member of the Boone Family (being the Boone family related to Gola Boone) any person related to Boone by marriage, or any know relative of a Boone-in-law.

#### Restriction:

Subject to covenants and restrictions of record including but not limited to access restrictions of the City of Bryant, Arkansas.



# ARKANSAS DEPARTMENT OF FINANCE AND ADMINISTRATION Arkansas Real Property Tax Affidavit of Compliance Form

Grantee (Purchaser) Name			Grantor (Seller) Name		
		Danny Daryl Anderson & Donna Faye Anderson			
Danny & Donna Anderson, Trustees Grantee (Purchaser) Address		Grantor (Seller) Address			
			, ,	:4	
298 W. Lawson Road	Chata	Zip Code	298 W. Lawson Road	State	Zip Code
City	State		1		
Alexander	AR	72002	Alexander	AR	72002
Date of real property transfer (as reflected or			/19		
Name of the county where the property is loc	Salin	e	interest (		
Amount of the full consideration for the trans	action: \$10.	00			
Tax is due: Value of the documentary	leration of \$10				
No tax is due: Exemption (check one e	evenihaon nei	Ovv)			
Any instrument given in  Any instrument solely for having been-paid at the having been-paid at the linstruments conveying Instruments, including the linstruments given by or agreement or order of the linstruments given in any the same person who is linstruments given to a linstruments conveying Department of Agricultus seller files with the country has owned a home with linstruments conveying shareholder, partner or distribution, or liquidated A beneficiary deed und	or the purpose time of the purpose time of the purpose time of the purpose time of the purpose time could be timber deeds, and party in a control of the court.  The party in a control of the purpose time the court.  The party in a control of the purpose time the court.  The party in a control of the purpose time the court.  The purpose time the purpose time the purpose time the purpose time time time time time time time tim	cure a debt.  e of correcting or representation of the revious recordation delinquent taxes.  erest in land only, which convey the relivorce action to othe ceeding to enforce anforce the security in lieu of or to avoince the security of deeds a sworn stream of the date of a corporation, partnership, 12-608.	ight to remove timber for a period not to exceed the party to the divorce action as a division of mather any security interest in real estate when the instr	excorded with further wenty-four (24) rital property warment transfer est in real estate Affairs, or Unit lars (\$60,000) er nor the spoule.	Il payment of tax  ) months.  hether by  s the property to  te.  ted States or less and the se of the buyer  ty and its
				- haa -l	an this ingle
	at documenta	ıry stamps or a doc	sumentary symbol in the legally correct amount ha	as deen placed	
Mary G. Nash			(Signature of Requestor)		3/18/19 (Date)

### **ACKNOWLEDGMENT**

STATE OF ARKANSAS	)	
	)	SS
COUNTY OF PULASKI	)	

On this day before me, a Notary Public, duly commissioned and acting, came Danny Daryl Anderson and Donna Faye Anderson, to me well known as (or satisfactorily proven to be) the Grantors in the foregoing deed, and stated that they executed the same for consideration, uses and purposes therein mentioned and set forth.

And Grantors declared that they have, of their own free will, executed said instrument for the consideration and purposes therein contained and set forth, without compulsion or undue influence.

WITNESS my hand and official seal this 18th day of 19th day of 19t

[Seal]

SHALLON A. SIGULINSKY
Notary Public-Arkansas
Pulaski County
My Commission Expires 05-18-2021
Commission # 12382559

Notary Public

My Commission Expires: 5.18.202

The undersigned hereby certifies under penalty of false swearing that the legally correct amount of documentary stamps has been placed on this instrument. Exempt or no consideration paid if none shown.

Grantee or Grantee's Agent

Grantee's Street Address

Grantee's City, State and Zip Code



October 9th, 2024

Re: Rezone Petition

A property located on Alcoa Road, Bryant, Arkansas is being considered for Rezoning on behalf of Stuart Finley from its current zoning as R - E to C - 3.

#### PARCELS # 840-15010-000

An application has been sent to the City of Bryant Planning Commission to rezone this parcel. As a part of this process a public hearing will be held November 11th, 2024 at 6:00 pm in the Boswell Municipal Complex at 210 SW 3<sup>rd</sup> Street, Bryant, AR 72022.

All parties interested in this matter may appear and be heard at the said time and place or may notify the Planning Commission of their views on this matter by letter or email. All persons interested in this request are invited to call or visit the Planning Office, City Administration Building to review and discuss the application with the planning staff.

Should you have any questions regarding this matter you may contact Hope Consulting at 501-315-2626 or the City of Bryant at 501-993-0999.

Thank you for your consideration in this process.

Sincerely,

Jonathan Hope







## SIGN PERMIT APPLICATION

Applicants are advised to read the Sign Ordinance prior to completing and signing this form.

The Sign Ordinance is available at <a href="www.cityofbryant.com">www.cityofbryant.com</a> under the Planning and Community

Development tab.

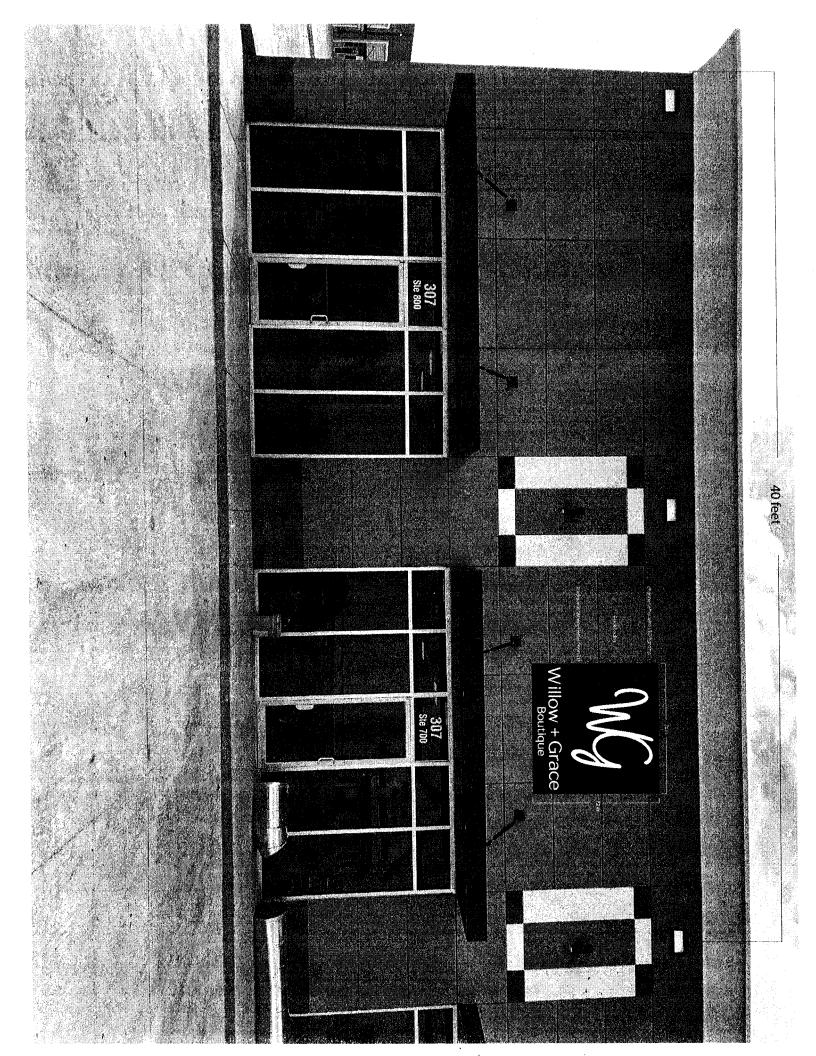
Developm	•
Date: 9/18/2024	Note: Electrical Permits may be Required, Please contact the Community Development Office for more information.
Sign Co. or Sign Owner	Property Owner
Name L. Graphic S Address 70/ N. Reynolds Rd City, State, Zip Bryant, AR72022 Phone (501) 653-4444 Email Address JOC @ L. Graphi x. Con	Name Bart Furguson  Address 307 progras Dr Ste. 700-800  City, State, Zip Bryant, AR7202 Z  Phone (SOI) 840-2282  Email Address bferg 620@Gorail: Com
GENERAL INFORMATION	•
Name of Business Willow + Grace Box Address/Location of sign 307 Progress dr	tique
Address/Location of sign 307 Progress de	ve Ste 700-800
Zoning Classification	
Please use following page to provide details on the provided on this application, a Site Plan showing pleasured to be submitted. Renderings of required to be submitted with the application. A the collected at the time of permit issuance. According special sign permit request shall be one hundred do required by Sign Administrator.	recement of sign(s) and any existing sign(s) on the fithe sign(s) showing the correct dimensions is also irty-five dollar (\$35) per sign payment will be to the Sign Ordinance a fee for and sign variance or
READ CAREFULLY BESORE SIGNING	

do hereby certify that all information contained within this application is true and correct. I fully understand that the terms of the Sign Ordinance supersede the Sign Administrator's approval and that all signs must fully comply with all terms of the Sign Ordinance regardless of approval. I further certify that the proposed sign is authorized by the owner of the property and that I am authorized by the property owner to make this application. I understand

that no sign may be placed in public right of way. I understand that I must comply with all Building and Electrical Codes and that it is my responsibility to obtain all necessary permits.

## Use table below to enter information regarding each sign for approval. Please use each letter to reference each sign rendering.

SIGN	<b>Type</b> (Façade, Pole, Monument, other)	<b>Dimensions</b> (Height, Length, Width)	Sqft (Measured in whole as rectangle)	Height of Sign (Measured from lot surface)		Column for Admin Certifying Approval
				Top of Sign	Bottom of Sign	
Α	wallsign	12" × 14"	36	19	13	
В						
С						
E						
F		and and communication and communication described to the communication of the communication o			Carlo and Product Company and the Manager of the Company of the Co	
G						





## City of Bryant, Arkansas Community Development 210 SW 3<sup>rd</sup> Street Bryant, AR 72022 501-943-0943

## SIGN PERMIT APPLICATION

Applicants are advised to read the Sign Ordinance prior to completing and signing this form.

The Sign Ordinance is available at <a href="https://www.cityofbryant.com">www.cityofbryant.com</a> under the Planning and Community

Development tab.

Date: 10/1/2024		Note: Electrical Permits may be Required, Please contact the Community Development Office for more information.
Sign Co. or Sign Owner	Property Owner	
Name L Graphics Address 70/ N. Reynolds Rd City, State, Zip Bryant, AR72022 Phone (501) 653-4444 Email Address TOC @ L Graphix, com	Name John  Address 5313  City, State, Zip Boy  Phone (501) 57  Email Address Jan	HW y 5 jant AR 72022
GENERAL INFORMATION		
Name of Business Bryant Mail and f	Print Center	
Name of Business Brigart Mail and F Address/Location of sign 5313 Hwy 5 8+e	. 305 - Biyan	t, AR72022
Zoning Classification	v	
Please use following page to provide details on the s	signs requesting appro	val. Along with information

Please use following page to provide details on the signs requesting approval. Along with information provided on this application, a Site Plan showing placement of sign(s) and any existing sign(s) on the property is required to be submitted. Renderings of the sign(s) showing the correct dimensions is also required to be submitted with the application. A thirty-five dollar (\$35) per sign payment will be collected at the time of permit issuance. According to the Sign Ordinance a fee for and sign variance or special sign permit request shall be one hundred dollars (\$100). Additional documentation may be required by Sign Administrator.

#### READ CAREFULLY BEFORE SIGNING

, do hereby certify that all information contained within this application is true and correct. I fully understand that the terms of the Sign Ordinance supersede the Sign Administrator's approval and that all signs must fully comply with all terms of the Sign Ordinance regardless of approval. I further certify that the proposed sign is authorized by the owner of the property and that I am authorized by the property owner to make this application. I understand

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SIGN	<b>Type</b> (Façade, Pole, Monument, other)	<b>Dimensions</b> (Height, Length, Width)	Sqft (Measured in whole as rectangle)	Height of Sign (Measured from lot surface)		Column for Admin Certifying Approval
				Top of Sign	Bottom of Sign	
Α	Wall G'sns	114" × 42"	33.6	20	16,5	•
В						
С						
E	THE DAY BOTTOM OF THE PERSON O	and the second s		AUGUSTO MALLE VICTORIA (MILLER PROPERTY AUGUSTO)		
F	The same of the sa			,		
G					e e e e e e e e e e e e e e e e e e e	

114 in



